

Montford Road #2-1  
County Highway

FIELD BOOK

307 T

PLEASE RETURN TO  
GEAUGA COUNTY ENGINEER  
COURT HOUSE  
CHARDON, O.  
PHONE 250-X

Box 22

County Road #24  
Mumford Cr. Road Imp.

Iron pipe were set all all  
PI & POT after pavement was  
laid

SEE INDEX NEXT PG.

MUMFORD RD Sec. A-B-C-D-  
E-F-G-H C.H. 24  
Align't., topo & sections 1-45  
Relocation Sta. 277 to end 48  
Drainage ditches 51-55  
Culverts 56-59  
Slopes & check levels 60-end

8.06 1120.40

3400	23	12	13	14	15	16	17	23
	6.3	6.5	7.5	7.2	7.0	6.8	6.2	6.2

2400	23	21	16	13	11	10	9	23
	5.2	5.2	6.0	5.4	5.2	4.8	5.4	4.8

1400	23	18	12	14	11	11	11	23
	4.5	4.7	4.8	4.2	4.1	4.8	4.2	4.6

0400	23	13	10	7	7	11	15	23
	1.9	2.6	3.1	2.6	2.1	2.5	3.0	1.8

1.42 1118.98

B.M. Nol.

Sta. 0+30

Spike in road 40"

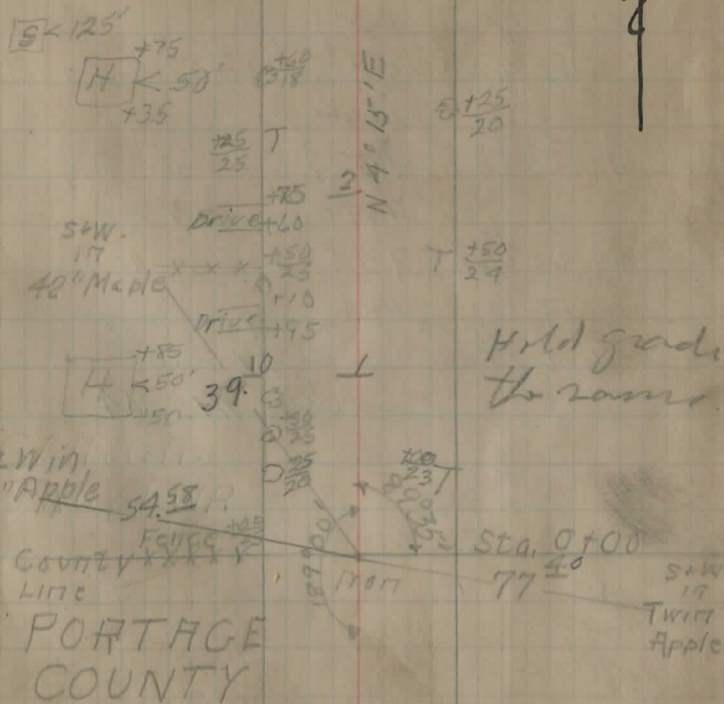
Maple 30 LE @

Profile South

50	100	150
2.1	2.1	2.5
3.7		

1218.3    1217.9    1216.7

T+15  
19 5 T+20  
23



Hold grade  
the same.

PORTAGE  
COUNTY

1104.6  
 11400  $\frac{230}{7.3}$   $\frac{13}{5.2}$   $\frac{11}{5.9}$   $\frac{9}{5.7}$   $\frac{13}{5.7}$   $\frac{15}{6.2}$   $\frac{19}{5.9}$   $\frac{230}{7.9}$

1104.9  
 10400  $\frac{230}{4.9}$   $\frac{13}{4.9}$   $\frac{9}{5.2}$   $\frac{11}{5.4}$   $\frac{11}{5.4}$   $\frac{14}{6.0}$   $\frac{15}{5.8}$   $\frac{230}{5.6}$

1105.3  
 7400  $\frac{230}{5.4}$   $\frac{13}{5.2}$   $\frac{11}{4.8}$   $\frac{9}{5.0}$   $\frac{11}{4.7}$   $\frac{11}{5.3}$   $\frac{230}{5.4}$   
 4.55 1105.74

7.18 1112.94

1106.0  
 8400  $\frac{230}{7.2}$   $\frac{15}{6.9}$   $\frac{13}{7.6}$   $\frac{9}{7.1}$   $\frac{9}{6.9}$   $\frac{7}{6.6}$   $\frac{10}{6.9}$   $\frac{13}{6.1}$   $\frac{230}{6.5}$

1107.1  
 7400  $\frac{230}{5.4}$   $\frac{14}{5.8}$   $\frac{13}{6.8}$   $\frac{10}{5.7}$   $\frac{10}{5.8}$   $\frac{8}{6.1}$   $\frac{10}{5.0}$   $\frac{13}{5.4}$   $\frac{22}{5.3}$   $\frac{25}{4.4}$

1108.4  
 6400  $\frac{230}{4.7}$   $\frac{16}{5.0}$   $\frac{14}{5.5}$   $\frac{11}{4.9}$   $\frac{11}{4.5}$   $\frac{6}{4.2}$   $\frac{7}{4.7}$   $\frac{13}{3.8}$   $\frac{230}{3.6}$

1109.9  
 5400  $\frac{230}{3.2}$   $\frac{17}{3.2}$   $\frac{16}{4.2}$   $\frac{13}{5.3}$   $\frac{11}{3.0}$   $\frac{5}{2.9}$   $\frac{9}{3.3}$   $\frac{11}{2.3}$   $\frac{21}{2.4}$   $\frac{25}{1.6}$

1111.6  
 4400  $\frac{230}{0.6}$   $\frac{18}{0.6}$   $\frac{15}{1.8}$   $\frac{12}{1.7}$   $\frac{9}{1.3}$   $\frac{5}{1.2}$   $\frac{9}{0.8}$   $\frac{25}{0.0}$   
 0.60 1112.34

B < 125'

H  $\frac{25}{40}$   
 405

can cut in  
 full 1 ft

S  $\frac{+40}{35}$   
 730

B  $\frac{+40}{30}$   
 720

H  $\frac{+20}{50}$   
 490

$\frac{+20}{20}$

T  $\frac{+40}{26}$

$\frac{+25}{20}$

$\frac{+40}{16}$

$\frac{+40}{18}$

11 X

25 >

X

X

X

X

X

X

X

X

X

X

X

X

X

X

X

X

X

X

X

X

X

X

X

X

X

X

X

X

X

X

X

X

X

X

X

X



1110.4

1110.39

104  
52  
A.6.

1104.7

23136	PL	H	G	K	G	H	FL	50	100	20
	12.4	59	61	37	20	58	121	123	128	12.5

1105.6

23100	25	14	11	8	4	9	12	15	25
	5.4	53	53	54	4.8	52	58	51	48

1108.3

22+00	25	11	7	4	14	18	25
	60	45	21	21	24	30	24

1109.9

21+60	25	6	5	4	11	13	25
	20	39	02	25	25	10	19

284 1110.39

11.90 1121.45

1113.2

21+00	25	19	11	4	6	9	15	25
	5.2	60	89	83	75	62	51	50

1117.9

20+00	25	11	9	4	8	10	11	15	30	25
	3.8	40	36	38	36	41	46	42	35	31

1116.3

19+00	25	12	7	2	4	9	11	25
	45	50	59	59	52	32	42	42

1112.9

18+00	25	9	7	3	4	10	11	13	25
	11	24	34	38	26	34	31	34	5.6

9.40 1112.05

2.79 1114.84

T<sup>50</sup><sub>19</sub>

Build new

10' 10'

Old Stone Culv.

Conc. Headwalls

1 slab.

6x4 Box

FAIR

Fair Cond.

23

22 0

22

175 [S]

130

T<sup>50</sup><sub>18</sub>

200

150 +

110

21

+00

S+W

17 18"

+85

MAPLE

S+W

11/13 Apple

58 32

45 13

75 20

T<sup>16</sup><sub>19</sub>

P I St 19+494

D AT LT 0°26'

S+W

17

APPLE

19

82.63

T<sup>10</sup><sub>14</sub>

27

18

33 12

S+W

SPKN. S. RE. APPLE

OPSCO POLE

Pipe Fd 4/24/40

AND RAISED WITH 1/2" IRON

ROD IN AUG '64

VERT S+W IN W. ROOT

24" MAPLE



1118.25

35400	25	19	12	9	113.0	5	7	10	17-19	21-25
	6.0	7.1	7.1	5.6	5.3	5.3	6.8	7.4		7.0

34400	25	14	9	112.4	8	10	25
	7.8	8.1	5.7	5.9	5.9	8.1	7.9

33439	FL	2	FL	50
	8.4	6.1	8.4	10.7

33400	25	15	9	112.8	33	23-25
	4.3	5.1	5.5	6.4	8.1	8.9

3.68 1114.57

32400	8.04	1122.61	117.0	13	17	25	30		
	2.0	2.7	6.0	5.5	5.6	6.2	8.7	11.3	14.4

31450	25	18	13	9	6	2	11	16	25	119.1		
	1.9	2.1	3.8	4.5	4.0	3.5	4.1	4.7	4.1	5.3		
BM#3										2.34	1120.27	1120.05
												1120.05

BM#3 2.11 1122.16 BM 1120.05

31400	25	16	11	7	118.0	8	8	14	19	25
	3.1	4.0	4.7	4.7	4.2	4.4	6.3	5.8	5.7	

30400	25	19	16	9	116.9	8	12	16	25
	4.7	5.3	6.3	5.2	5.3	5.7	6.9	6.1	5.8

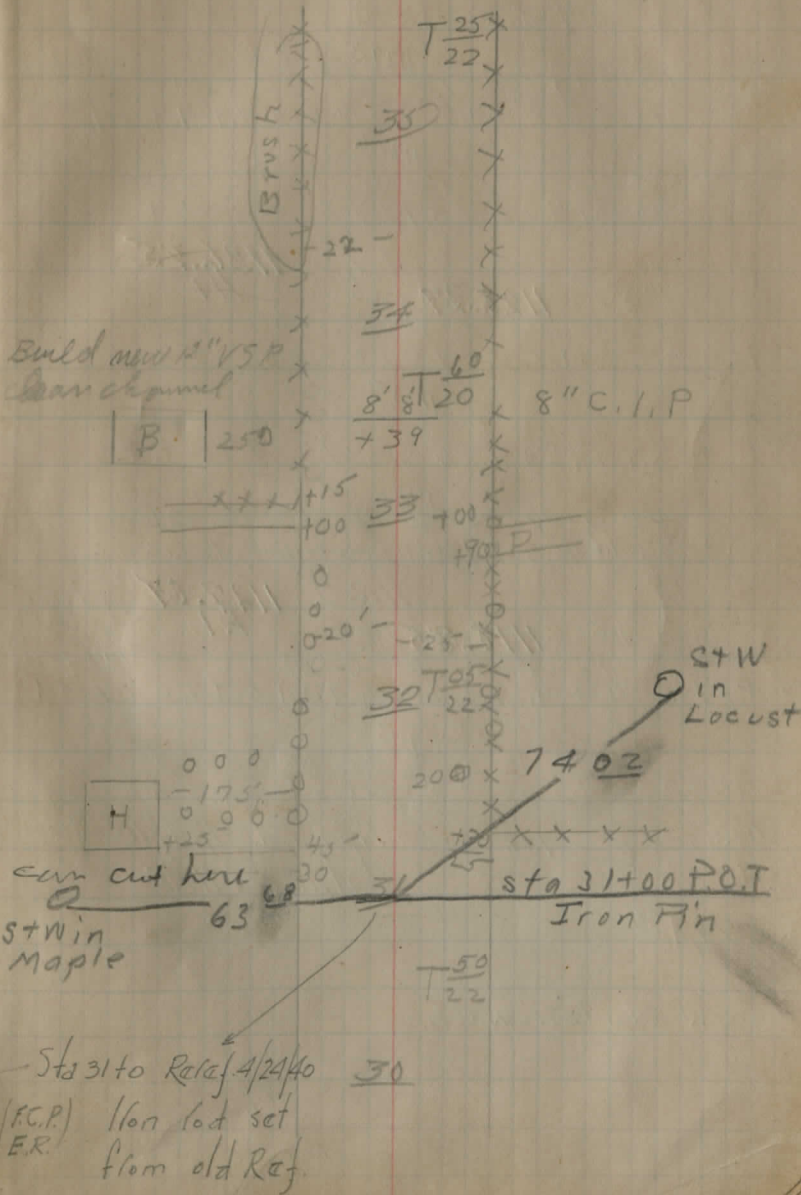
Seq W; S side 10' Loc.

Seq W in S side 14' Map. 1.5' up

63.68

65.62

82.48 Seq W; W side O.P.S pole





1141.1

47+00  $\frac{25}{2.5}$   $\frac{18}{2.4}$   $\frac{14}{9.8}$   $\frac{8}{8.9}$   $\frac{8}{8.8}$   $\frac{5}{8.6}$   $\frac{6}{9.6}$   $\frac{11}{8.1}$   $\frac{18-25}{5.1}$

B74 A 18.34 10.34 11.39.35 1139.49

0.40 1139.89 1138.0

46+40  $\frac{25}{1.1}$   $\frac{17}{1.2}$   $\frac{14}{2.9}$   $\frac{12}{1.8}$   $\frac{8}{1.9}$   $\frac{7}{1.4}$   $\frac{8}{2.5}$   $\frac{13}{1.3}$   $\frac{19}{1.5}$   $\frac{25}{2.3}$

46+00  $\frac{25}{2.3}$   $\frac{16}{3.8}$   $\frac{14}{3.0}$   $\frac{11}{3.2}$   $\frac{5}{3.0}$   $\frac{5}{4.2}$   $\frac{7-9}{2.8}$   $\frac{11}{3.2}$   $\frac{25}{3.2}$

1134.7

45+00  $\frac{25}{3.6}$   $\frac{18}{5.2}$   $\frac{16}{5.5}$   $\frac{15}{5.0}$   $\frac{8}{5.2}$   $\frac{6}{5.0}$   $\frac{8}{5.8}$   $\frac{10}{4.9}$   $\frac{14}{5.4}$   $\frac{25}{5.4}$

1133.0

44+00  $\frac{23}{7.5}$   $\frac{20}{7.0}$   $\frac{19}{7.3}$   $\frac{18}{6.9}$   $\frac{8}{6.9}$   $\frac{6-9}{8.3}$   $\frac{13-14}{11.6}$   $\frac{19}{9.2}$   $\frac{25}{7.6}$

Bridge

43+45  $\frac{13}{11.8}$   $\frac{10}{10.9}$   $\frac{50}{11.3}$  FL  $\frac{13}{7.9}$   $\frac{8}{8.0}$   $\frac{1}{8.0}$  FL  $\frac{50}{11.8}$   $\frac{100}{11.3}$   $\frac{100}{8.9}$

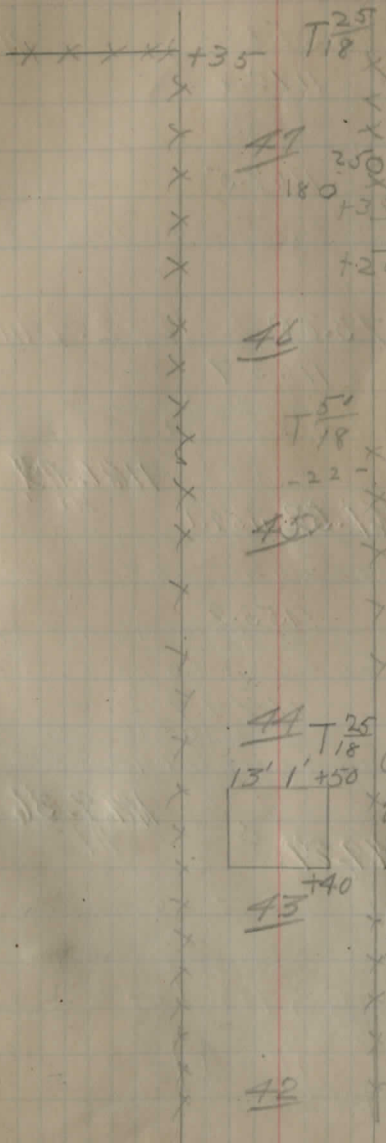
9.22 1130.67

0.80 1131.47 1129.4

43+00  $\frac{23}{2.3}$   $\frac{15}{2.0}$   $\frac{10}{2.7}$   $\frac{8}{2.1}$   $\frac{6}{2.8}$   $\frac{7-8}{3.6}$   $\frac{13}{2.7}$   $\frac{23}{1.8}$

1126.9

42+00  $\frac{25}{3.6}$   $\frac{18}{7.8}$   $\frac{15}{4.6}$   $\frac{10}{3.7}$   $\frac{8}{4.6}$   $\frac{4}{4.5}$   $\frac{8}{3.7}$   $\frac{9}{4.8}$   $\frac{14}{4.1}$   $\frac{25}{3.5}$



Sta. 40 to 53  
incl. recross  
sect. (see pg. 46)

Old Wood Plank Bridge  
12' Clearance  
Very Poor Cond.  
Fl. Lt.  
36" Cur. Pipe 80° R+H  
36' long

0.11 1173.55  
 BM# 0.61 1173.55 1172.94

1170.8  
 54+00  $\frac{25}{23} \frac{18}{26} \frac{13}{34} \frac{8}{33} \frac{4}{28} \frac{5}{34} \frac{10}{36} \frac{13}{24} \frac{25}{24}$

1167.5  
 53+00  $\frac{25}{42} \frac{19}{53} \frac{14}{69} \frac{10}{70} \frac{4}{67} \frac{5}{61} \frac{9}{64} \frac{12}{57} \frac{17}{43} \frac{25}{32}$

B.M.#5  
 0.06 1173.00 1172.94 1172.94

1163.7  
 52+00  $\frac{25}{6.6} \frac{15}{9.0} \frac{16}{10.8} \frac{11}{9.9} \frac{7}{9.3} \frac{5}{9.6} \frac{10}{11.1} \frac{13}{8.5} \frac{15}{6.8} \frac{25}{6.2}$

11.81 1161.19  
 0.33 1161.52 1159.1  
 51+00  $\frac{25-23}{-1.6} \frac{10}{3.5} \frac{9}{2.3} \frac{7}{2.4} \frac{6}{2.9} \frac{8}{3.8} \frac{10}{2.3} \frac{13}{2.2} \frac{20}{-0.5} \frac{25}{-0.7}$

1153.9  
 50+00  $\frac{25}{7.8} \frac{21}{5.1} \frac{15}{8.9} \frac{6}{4.6} \frac{7}{7.6} \frac{9}{7.9} \frac{9}{9.0} \frac{12}{7.3} \frac{15}{7.3} \frac{19}{5.9} \frac{25}{5.5}$

1149.9  
 49+00  $\frac{25}{9.7} \frac{19}{9.8} \frac{12}{12.8} \frac{7}{11.9} \frac{9}{11.6} \frac{7}{11.6} \frac{10}{12.9} \frac{15}{11.0} \frac{25}{9.8}$   
 12.16 1149.36

0.53 1149.89 1145.5  
 48+00  $\frac{20}{2.1} \frac{15}{3.4} \frac{11}{5.7} \frac{6}{4.4} \frac{4}{4.4} \frac{5}{7.6} \frac{8}{5.7} \frac{13}{3.0} \frac{25}{2.3}$

Sta. 40 to 53 incl.  
 See pg. 46-47

28 70  
 +30  
 +15  
 53  
 +60  
 +45  
 T +40  
 20  
 +40  
 300  
 +85  
 +50  
 300  
 can cut some here.  
 32  
 51  
 T +75  
 19  
 50  
 49 T 00  
 19  
 48

0.63 1184.25 1183.6  
 59+00  $\frac{25}{1.1} \frac{20}{1.2} \frac{13}{1.3} \frac{8}{0.8} \frac{8}{0.7} \frac{12}{1.4} \frac{12}{1.7} \frac{19}{1.2} \frac{25}{-1.5} \frac{25}{-1.8}$

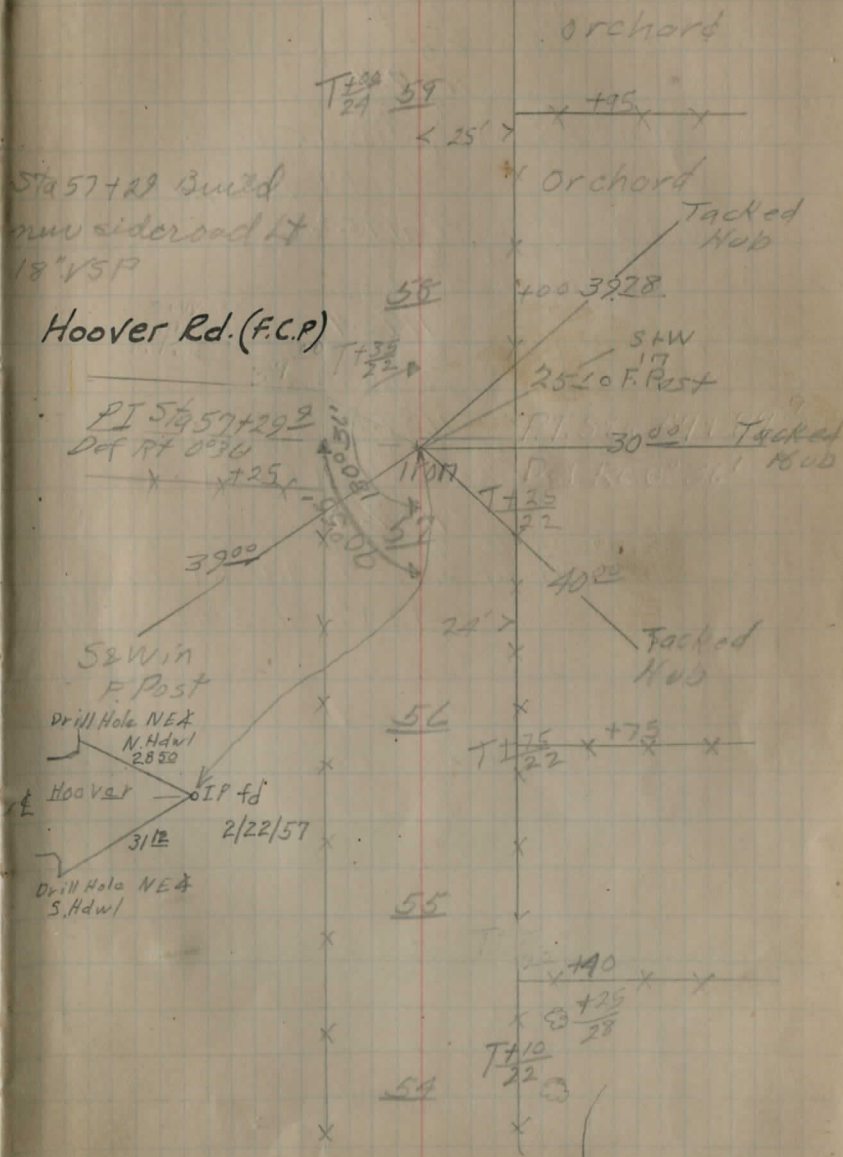
1180.4  
 58+00  $\frac{25}{2.8} \frac{16}{3.5} \frac{12}{4.4} \frac{8}{3.9} \frac{7}{4.4} \frac{19}{3.2} \frac{25}{2.6}$

Road Intersection 1178.0  
 $\frac{150}{6.3} \frac{100}{5.4} \frac{50}{5.2} \frac{25}{5.8} \frac{8}{6.3}$

1177.4  
 57+00  $\frac{25}{7.0} \frac{16}{7.7} \frac{12}{7.8} \frac{8}{6.9} \frac{6}{7.2} \frac{11}{7.0} \frac{12}{6.5} \frac{25}{6.3}$

1175.0  
 56+00  $\frac{25}{9.6} \frac{15}{9.3} \frac{8}{9.4} \frac{8}{9.3} \frac{6}{9.4} \frac{9}{9.5} \frac{11}{9.0} \frac{25}{9.0}$

1173.2  
 55+00  $\frac{25}{11.2} \frac{19}{11.2} \frac{8}{11.6} \frac{8}{11.1} \frac{4}{11.5} \frac{8}{11.8} \frac{12}{10.7} \frac{25}{11.1}$   
 11.28 1172.97 1172.94



1199.9

65+00	$\frac{25}{6.7}$	$\frac{19}{7.0}$	$\frac{15}{8.6}$	$\frac{11}{8.8}$	$\frac{9}{8.5}$	$\frac{8}{8.8}$	$\frac{10}{9.2}$	$\frac{8}{8.4}$	$\frac{25}{7.1}$
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1197.4

64+00	$\frac{25}{9.7}$	$\frac{19}{10.9}$	$\frac{15}{11.5}$	$\frac{13}{11.4}$	$\frac{9}{11.0}$	$\frac{5}{11.3}$	$\frac{7}{11.5}$	$\frac{8}{11.0}$	$\frac{25}{9.5}$
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12.47 1195.91

0.13 1196.04 1195.2

63+00	$\frac{25}{-1.0}$	$\frac{19}{0.7}$	$\frac{13}{1.4}$	$\frac{14}{1.2}$	$\frac{9}{0.8}$	$\frac{6}{1.0}$	$\frac{8}{1.2}$	$\frac{25}{0.60}$
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1192.4

62+00	$\frac{25}{2.2}$	$\frac{18}{3.0}$	$\frac{15}{4.3}$	$\frac{13}{3.8}$	$\frac{6}{3.6}$	$\frac{8}{4.0}$	$\frac{14}{4.0}$	$\frac{25}{2.9}$	$\frac{25}{2.2}$
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1189.8

61+00	$\frac{25}{4.6}$	$\frac{19}{5.2}$	$\frac{13}{6.9}$	$\frac{10}{6.3}$	$\frac{9}{6.2}$	$\frac{5}{6.6}$	$\frac{8}{7.1}$	$\frac{14}{6.8}$	$\frac{25}{5.4}$	$\frac{25}{5.2}$
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1187.3

60+00	$\frac{25}{7.0}$	$\frac{19}{7.5}$	$\frac{11}{9.4}$	$\frac{9}{9.1}$	$\frac{9}{8.7}$	$\frac{5}{9.0}$	$\frac{7}{9.8}$	$\frac{12}{7.2}$	$\frac{17}{7.7}$	$\frac{25}{7.0}$
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12.42 1183.62

x

x

+25	x	+75	x
14	< 100		
	+90		

775

760

$$\frac{T+10}{22}$$

64

Can cut here if possible.

65

$$\frac{T+65}{22}$$
+45  
+38

62

125' &gt;

+70	H
+75	

23	x	+60	x	x
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61

orchard

$$\frac{T+70}{22}$$

60



1.67 1224.72

78+00	25	11	8	5	9	13	14	25
	1.5	1.9	2.5	2.1	1.7	2.3	2.6	2.2
								1.5

1221.3

77+00	25	9	5	3	10	12	25
	4.3	4.5	3.9	3.4	3.8	4.5	4.2

1220.2

76+00	25	7	4	8	11	16	25
	6.2	6.0	5.4	4.5	4.8	6.1	6.8

1219.7

75+00	25	12	5	3	8	15	25
	5.6	5.5	5.8	5.0	5.0	5.8	5.4

1220.1

74+00	25	9	4	3	6	11	13	19	25
	4.8	5.5	5.2	4.6	4.5	5.2	6.3	4.8	4.4

1217.0

73+00	25	15	10	5	4	11	14	25
	8.2	8.6	9.2	8.1	7.7	8.0	8.7	8.3
								6.8

8.22 1216.50

T+35

17

<20>

T+75

28

<28>

28

<28>

77

T+95

19

T+13

22

76

Drainage ditch  
at Wat 76+00

75

T+50

18

74

73

T+70

18

<28>

<30>

Brush

+50

x

C. in road  
about Sta. 74+50

x

x

x

T+50

30

T+02

28

x

Brush

x

x

x

+95

x

x

x

x



1.86 1241.28

	25	18	19	6	9	6	7	25	
91+00	2.0	2.1	2.7	3.6	2.7	2.9	3.7	1.9	

1237.1

	25	15	7	6	10	14	25		
90+00	4.6	4.8	5.3	4.2	4.2	4.9	4.8		

1236.4

	25	16	12	6	8	9	13	25	
89+00	6.6	6.7	6.7	4.7	4.9	4.9	6.5	6.3	

1236.3

	16	50	FL	8	FL				
88+74	9.3	8.2	7.4	5.0	7.3				

1235.7

	25	16	11	6	8	13	16	25	
88+00	7.0	7.1	7.3	5.5	5.6	5.5	6.9	7.0	6.8

1236.2

	25	19	13	6	7	14	19	25	
87+00	7.2	7.2	6.6	5.4	5.1	5.5	7.8	7.3	6.4

1236.6

	25	12	8	8	7	13	19	25	
86+00	6.5	6.6	5.2	4.7	5.0	6.4	5.0	5.0	

5.55 1235.73

91

T 25  
24

25 90

End. Min. E.

25 89

Build new 18" CP  
SP Branch and  
50' Lt.

8' 10  
+74

12" Corr. Pipe  
Fl. LL

+50  
25

88

+40

+15

87

Cemetery

+60  
25

50 \* +20

86

1249.01

1243.2

98+00	$\frac{25}{4.1}$	$\frac{14}{4.5}$	$\frac{8}{6.7}$	$\frac{8}{5.8}$	$\frac{8}{5.9}$	$\frac{14}{6.9}$	$\frac{19}{4.4}$	$\frac{25}{4.5}$
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1240.3

97+00	$\frac{25}{7.1}$	$\frac{13}{7.5}$	$\frac{9}{9.0}$	$\frac{7}{9.3}$	$\frac{9}{8.7}$	$\frac{9}{8.9}$	$\frac{12}{10.2}$	$\frac{15}{10.4}$	$\frac{20-25}{7.0}$
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1238.1

96+00	$\frac{25}{7.2}$	$\frac{12}{7.6}$	$\frac{9}{12.4}$	$\frac{9}{10.9}$	$\frac{9}{11.1}$	$\frac{14}{11.5}$	$\frac{17}{11.3}$	$\frac{25}{11.3}$
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10.82 1238.19

4.80 1242.99

1237.1

95+00	$\frac{25}{7.1}$	$\frac{13}{6.7}$	$\frac{6}{6.4}$	$\frac{9}{5.9}$	$\frac{11}{5.9}$	$\frac{15}{6.2}$	$\frac{17}{5.8}$	$\frac{25}{6.6}$
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1287.5

94+70	$\frac{100}{9.0}$	$\frac{50}{8.6}$	$\frac{4}{7.2}$	$\frac{6}{5.7}$	$\frac{9}{5.3}$	$\frac{9}{5.4}$	$\frac{4}{4.3}$	$\frac{FL}{8.5}$
-------	-------------------	------------------	-----------------	-----------------	-----------------	-----------------	-----------------	------------------

1237.7

94+00	$\frac{25}{6.6}$	$\frac{13}{6.1}$	$\frac{2}{5.9}$	$\frac{9}{5.3}$	$\frac{7}{5.7}$	$\frac{11}{6.3}$	$\frac{15}{5.7}$	$\frac{25}{4.6}$
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1239.6

93+00	$\frac{25}{2.4}$	$\frac{15}{2.5}$	$\frac{9}{4.5}$	$\frac{6}{3.4}$	$\frac{5}{3.7}$	$\frac{10}{4.3}$	$\frac{13}{3.5}$	$\frac{20}{1.8}$	$\frac{25}{1.5}$
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1241.0

92+00	$\frac{25}{3.0}$	$\frac{10}{2.5}$	$\frac{8}{3.1}$	$\frac{9}{2.0}$	$\frac{6}{2.2}$	$\frac{11}{3.2}$	$\frac{14}{2.1}$	$\frac{21}{0.7}$	$\frac{25}{0.5}$
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3.57 1239.42

$\frac{60}{21}$   
 $\frac{40}{21}$

< 25'

98

$\frac{150}{21}$

97

$\frac{150}{23}$

$\frac{60}{22}$

100

96

95

Build new  
3x2 Conc Box  
diam channel.

Old Stone Culv.  
3x2 Box  
FL Lt.  
Good Cond.

$\frac{9}{14}$   
+70

$\frac{60}{24}$

94

$\frac{100}{10}$

93

$\frac{60}{23}$

92

1248.93

1244.4

104+00  $\frac{25}{5.2}$   $\frac{13}{5.0}$   $\frac{11}{5.8}$   $\frac{9}{5.2}$   $\frac{8}{4.5}$   $\frac{11}{5.4}$   $\frac{15}{6.0}$   $\frac{19}{4.5}$   $\frac{25}{3.6}$

1244.2

103+00  $\frac{25}{5.4}$   $\frac{14}{3.4}$   $\frac{9}{5.5}$   $\frac{6}{5.1}$   $\frac{9}{4.7}$   $\frac{2}{4.6}$   $\frac{13}{6.1}$   $\frac{19}{5.1}$   $\frac{25}{4.4}$

1244.1

102+00  $\frac{25}{4.5}$   $\frac{13}{5.1}$   $\frac{10}{5.3}$   $\frac{6}{5.1}$   $\frac{2}{4.8}$   $\frac{11}{4.9}$   $\frac{13}{5.6}$   $\frac{17}{5.0}$   $\frac{25}{4.0}$

B.M. #10 1246.86

8.60 1249.46

1245.5

101+00  $\frac{25}{3.9}$   $\frac{14}{3.8}$   $\frac{11}{4.8}$   $\frac{8}{4.0}$   $\frac{9}{4.1}$   $\frac{12}{5.1}$   $\frac{15}{5.7}$   $\frac{16}{4.8}$   $\frac{25}{3.8}$

4.00 1245.46

3.55 1249.01 1244.7 1245.1

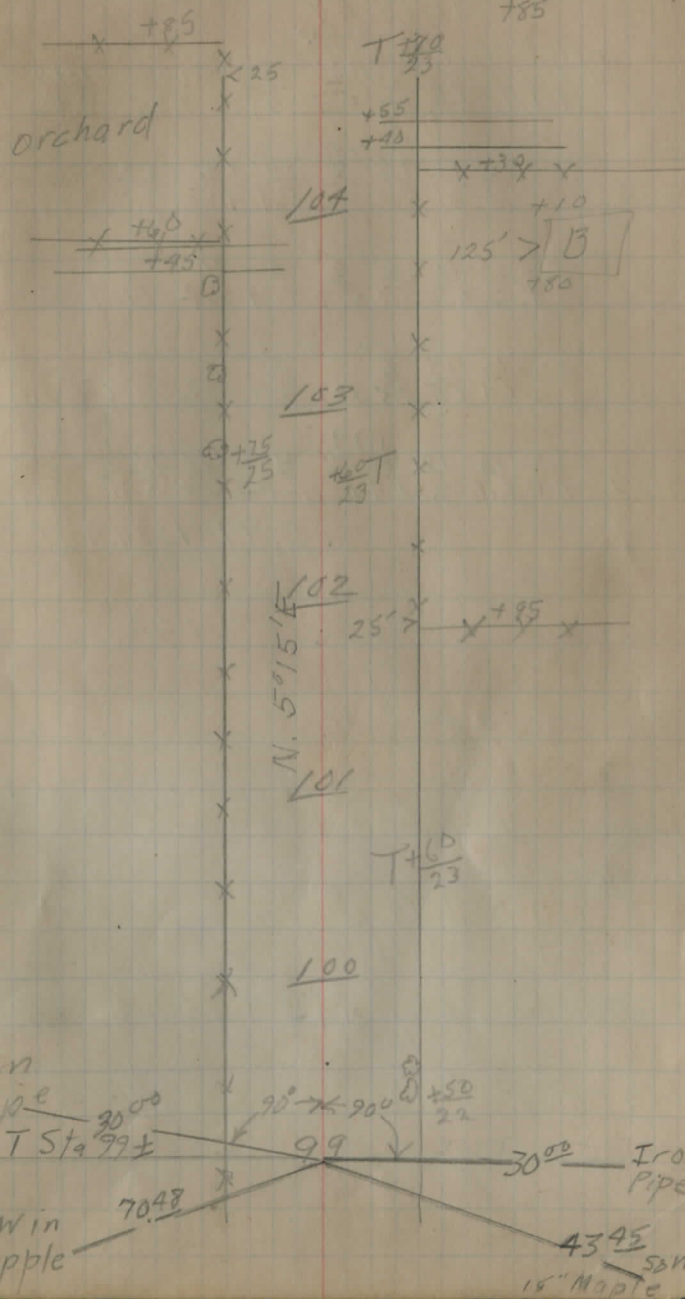
100+00  $\frac{25}{4.2}$   $\frac{13}{4.3}$   $\frac{9}{4.9}$   $\frac{10}{4.3}$   $\frac{8}{4.3}$   $\frac{9}{4.7}$   $\frac{14}{7.5}$   $\frac{25}{7.5}$

1245.6

99+00  $\frac{25}{5.3}$   $\frac{19}{4.0}$   $\frac{12}{4.7}$   $\frac{8}{4.3}$   $\frac{2}{5.4}$   $\frac{7}{3.5}$   $\frac{14}{4.8}$   $\frac{17}{4.8}$   $\frac{29}{3.4}$   $\frac{25}{3.1}$

BM #9 3.02 1245.99 1246.01

70°  $\times$  H  $\frac{+20}{785}$







9.97 1261.54 <sup>1252.6</sup>  
 118+00  $\frac{25}{6.6} \frac{17}{7.2} \frac{10}{11.6} \frac{2}{9.5} \frac{8}{8.9} \frac{4}{9.4} \frac{8}{11.2} \frac{17}{6.4} \frac{25}{6.2}$

<sup>25</sup>  
 119+00  $\frac{220}{4.2} \frac{13}{8.0} \frac{10}{6.8} \frac{2}{6.0} \frac{1255.4}{6.1} \frac{14}{6.9} \frac{7}{8.3} \frac{14}{4.2} \frac{25}{3.9}$

120+00  $\frac{25}{3.2} \frac{17}{3.5} \frac{15}{5.0} \frac{13}{4.2} \frac{7}{3.7} \frac{1258.1}{3.7} \frac{4}{4.4} \frac{6}{5.3} \frac{8}{4.0} \frac{15}{3.0} \frac{25}{3.0}$

121+00  $\frac{25}{2.2} \frac{17}{2.4} \frac{14}{2.8} \frac{8}{5.0} \frac{1259.6}{1.9} \frac{5}{2.8} \frac{8}{4.0} \frac{9}{2.6} \frac{14}{1.5} \frac{25}{1.3}$

0.75 - 1260.79

10.20 1270.99 1260.7  
 122+00  $\frac{23}{9.2} \frac{2}{9.3} \frac{13}{11.6} \frac{8}{10.3} \frac{5}{10.3} \frac{3}{10.9} \frac{6}{11.6} \frac{15}{8.4} \frac{25}{8.0}$

123+00  $\frac{25}{6.5} \frac{17}{7.1} \frac{14}{9.4} \frac{6}{7.6} \frac{1263.4}{7.6} \frac{5}{8.5} \frac{7}{9.6} \frac{15}{5.6} \frac{25}{5.7}$

124  
 X <20 18> X

X 123 X

X 122 X

X 121 X

X 120 X

X 119 X

Brush X <15 18> Brush

X 118 X

$\frac{125}{25}$

12659

124+00  $\frac{25}{4.0}$   $\frac{15}{5.8}$   $\frac{13}{2.0}$   $\frac{5}{5.2}$   $\frac{9}{5.1}$   $\frac{4}{1.5}$   $\frac{8}{7.4}$   $\frac{11}{5.4}$   $\frac{15}{4.2}$   $\frac{25}{4.2}$

12681

125+00  $\frac{25}{2.6}$   $\frac{20}{3.5}$   $\frac{14}{4.3}$   $\frac{11}{3.3}$   $\frac{5}{2.9}$   $\frac{5}{3.7}$   $\frac{9}{5.4}$   $\frac{12}{3.5}$   $\frac{20}{3.8}$

B.M #12 2.637 1268.32 1268.27

5.07 1273.34 12691

126+00  $\frac{25}{4.7}$   $\frac{13}{5.5}$   $\frac{8}{4.9}$   $\frac{4}{4.2}$   $\frac{5}{5.1}$   $\frac{6}{5.9}$   $\frac{9}{5.2}$   $\frac{11}{5.2}$   $\frac{25}{5.2}$

12694

127+00  $\frac{25}{4.0}$   $\frac{14}{4.6}$   $\frac{13}{4.9}$   $\frac{9}{4.7}$   $\frac{7}{3.9}$   $\frac{6}{4.9}$   $\frac{9}{5.4}$   $\frac{11}{4.8}$   $\frac{25}{4.7}$

12700

128+00  $\frac{25}{4.0}$   $\frac{13}{4.2}$   $\frac{8}{3.8}$   $\frac{4}{3.3}$   $\frac{5}{4.0}$   $\frac{9}{4.8}$   $\frac{11}{4.2}$   $\frac{25}{4.2}$

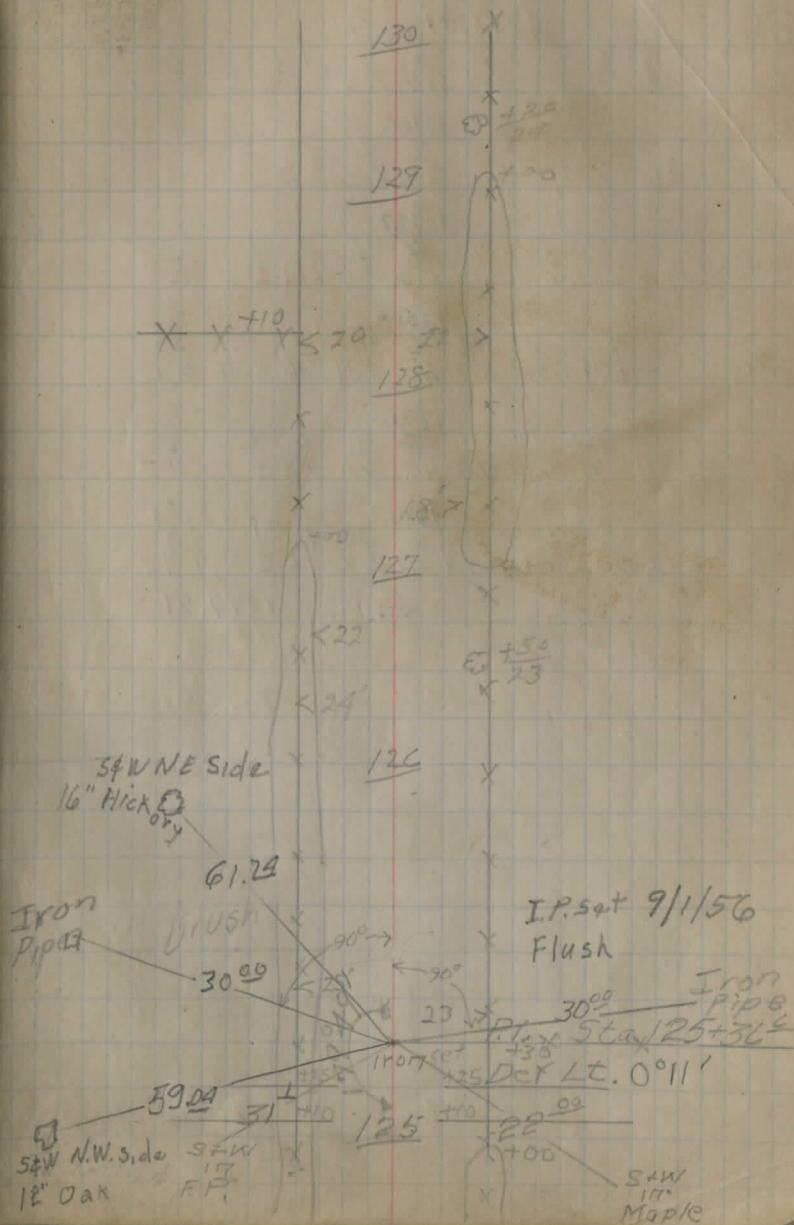
1270.3

129+00  $\frac{25}{2.8}$   $\frac{17}{2.5}$   $\frac{13}{4.5}$   $\frac{6}{3.5}$   $\frac{5}{3.0}$   $\frac{6}{3.7}$   $\frac{9}{4.3}$   $\frac{11}{3.7}$   $\frac{18}{3.1}$   $\frac{25}{3.0}$

12703

130+00  $\frac{25}{3.3}$   $\frac{13}{3.8}$   $\frac{7}{3.2}$   $\frac{4}{3.0}$   $\frac{6}{3.3}$   $\frac{10}{3.8}$   $\frac{12}{3.5}$   $\frac{25}{3.4}$

2.81 1270.53



5.78 1276.31 1270.4  
25 14 9 8 6 9 11 25  
131+00 6.4 6.3 6.4 5.9 6.5 7.0 6.5 6.4

1270.4  
25 16 13 7 6 10 25  
132+00 6.4 6.3 6.5 6.2 5.9 6.3 6.2 6.3

1270.7  
25 15 13 10 8 5 8 9 25  
133+00 6.3 6.0 6.1 6.0 5.6 6.0 6.4 5.8 6.2

1271.4  
25 13 9 8 4 6 9 25  
134+00 5.4 5.8 5.3 4.9 5.4 5.6 5.4 4.9

1272.2  
25 22 14 9 8 6 10 25  
135+00 4.2 4.2 4.8 4.6 4.1 4.6 4.8 4.3 3.3

1273.2  
25 19 16 9 8 3 11 18 25  
136+00 2.8 3.2 3.9 3.4 3.1 3.4 3.6 2.5 1.7 1.8  
2.10 1274.21

136

~~135~~

~~134~~

~~133~~

~~132~~

25 x +90 x x x

~~131~~

7.90 1282.11 1274.4  
 137+00  $\begin{array}{r} 25 \\ 7.4 \end{array}$   $\begin{array}{r} 19 \\ 7.6 \end{array}$   $\begin{array}{r} 15 \\ 8.4 \end{array}$   $\begin{array}{r} 11 \\ 8.2 \end{array}$   $\begin{array}{r} 7 \\ 7.7 \end{array}$   $\begin{array}{r} 10 \\ 8.1 \end{array}$   $\begin{array}{r} 25 \\ 7.3 \end{array}$   $\begin{array}{r} 25 \\ 6.8 \end{array}$

138+00  $\begin{array}{r} 25 \\ 6.4 \end{array}$   $\begin{array}{r} 20 \\ 6.4 \end{array}$   $\begin{array}{r} 13 \\ 7.5 \end{array}$   $\begin{array}{r} 9 \\ 7.0 \end{array}$   $\begin{array}{r} 1275.4 \\ 6.7 \end{array}$   $\begin{array}{r} 5 \\ 7.0 \end{array}$   $\begin{array}{r} 8 \\ 7.1 \end{array}$   $\begin{array}{r} 12 \\ 6.4 \end{array}$   $\begin{array}{r} 25 \\ 5.9 \end{array}$

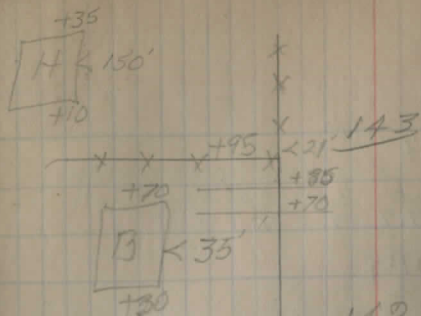
139+00  $\begin{array}{r} 25 \\ 6.2 \end{array}$   $\begin{array}{r} 19 \\ 6.2 \end{array}$   $\begin{array}{r} 14 \\ 6.8 \end{array}$   $\begin{array}{r} 10 \\ 6.5 \end{array}$   $\begin{array}{r} 1276.1 \\ 6.0 \end{array}$   $\begin{array}{r} 4 \\ 6.3 \end{array}$   $\begin{array}{r} 8 \\ 6.6 \end{array}$   $\begin{array}{r} 10 \\ 6.2 \end{array}$   $\begin{array}{r} 25 \\ 5.7 \end{array}$

140+00  $\begin{array}{r} 25 \\ 4.9 \end{array}$   $\begin{array}{r} 10 \\ 5.6 \end{array}$   $\begin{array}{r} 13 \\ 6.2 \end{array}$   $\begin{array}{r} 9 \\ 5.8 \end{array}$   $\begin{array}{r} 1276.7 \\ 5.4 \end{array}$   $\begin{array}{r} 6 \\ 6.0 \end{array}$   $\begin{array}{r} 7 \\ 6.1 \end{array}$   $\begin{array}{r} 13 \\ 5.6 \end{array}$   $\begin{array}{r} 25 \\ 4.7 \end{array}$

141+00  $\begin{array}{r} 23 \\ 5.1 \end{array}$   $\begin{array}{r} 16 \\ 5.1 \end{array}$   $\begin{array}{r} 13 \\ 6.1 \end{array}$   $\begin{array}{r} 9 \\ 5.4 \end{array}$   $\begin{array}{r} 1277.2 \\ 4.9 \end{array}$   $\begin{array}{r} 5 \\ 5.3 \end{array}$   $\begin{array}{r} 9 \\ 5.8 \end{array}$   $\begin{array}{r} 11 \\ 5.2 \end{array}$   $\begin{array}{r} 25 \\ 4.6 \end{array}$

B.M. #13  
 142+00  $\begin{array}{r} 25 \\ 5.8 \end{array}$   $\begin{array}{r} 13 \\ 6.6 \end{array}$   $\begin{array}{r} 10 \\ 6.3 \end{array}$   $\begin{array}{r} 9 \\ 5.7 \end{array}$   $\begin{array}{r} 1276.4 \\ 6.3 \end{array}$   $\begin{array}{r} 5 \\ 6.5 \end{array}$   $\begin{array}{r} 9 \\ 5.5 \end{array}$   $\begin{array}{r} 13 \\ 4.7 \end{array}$   $\begin{array}{r} 1278.14 \\ 1278.13 \end{array}$

143+00  $\begin{array}{r} 25 \\ 6.3 \end{array}$   $\begin{array}{r} 12 \\ 6.6 \end{array}$   $\begin{array}{r} 14 \\ 7.5 \end{array}$   $\begin{array}{r} 11 \\ 6.9 \end{array}$   $\begin{array}{r} 1275.5 \\ 6.6 \end{array}$   $\begin{array}{r} 5 \\ 7.0 \end{array}$   $\begin{array}{r} 11 \\ 7.2 \end{array}$   $\begin{array}{r} 15 \\ 6.3 \end{array}$   $\begin{array}{r} 25 \\ 6.0 \end{array}$   
 6.40 1275.71



142

141

140

139

138

137

1278.92 1274.2  
 3.21 Road Intersection  
 143+90  $\frac{150}{8.4}$   $\frac{100}{7.4}$   $\frac{50}{6.1}$   $\frac{25}{5.5}$   $\frac{0}{4.7}$   $\frac{25}{4.4}$   $\frac{50}{4.0}$   $\frac{100}{3.5}$

1273.9  
 144+00  $\frac{25}{5.9}$   $\frac{0}{5.0}$   $\frac{25}{3.7}$

1274.4  
 145+00  $\frac{25}{4.5}$   $\frac{19}{4.7}$   $\frac{16}{5.1}$   $\frac{13}{5.0}$   $\frac{0}{4.5}$   $\frac{4}{4.8}$   $\frac{7}{5.1}$   $\frac{13}{4.4}$   $\frac{25}{3.1}$

1273.8  
 146+00  $\frac{25}{3.0}$   $\frac{13}{6.0}$   $\frac{13}{5.6}$   $\frac{0}{5.1}$   $\frac{5}{5.4}$   $\frac{9}{5.3}$   $\frac{16}{4.3}$   $\frac{25}{3.7}$

1272.9  
 147+00  $\frac{25}{5.8}$   $\frac{21}{5.8}$   $\frac{16}{6.6}$   $\frac{0}{6.0}$   $\frac{0}{6.8}$   $\frac{7}{6.4}$   $\frac{11}{6.0}$   $\frac{25}{4.6}$

1272.2  
 148+00  $\frac{25}{2.5}$   $\frac{22}{2.6}$   $\frac{14}{7.2}$   $\frac{0}{6.7}$   $\frac{0}{6.7}$   $\frac{5}{7.4}$   $\frac{8}{6.7}$   $\frac{25}{6.3}$   
 BM "14 6.21 1272.71 1272.70

18'x20' R turnouts at Nash

Profile N

East

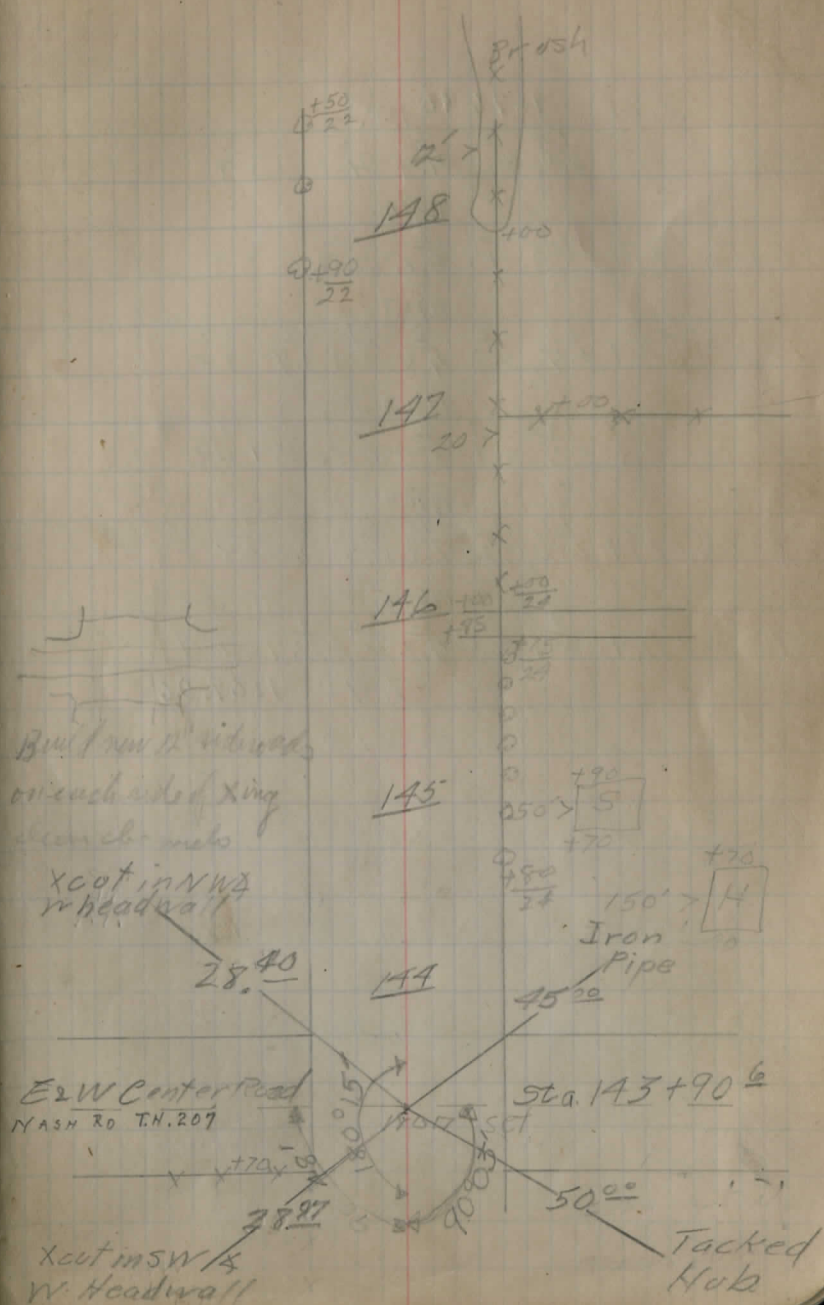
0 to	1+0	2+0	3+0	4+0	5+0	6+0
1.5	1.2	1.4	3.2	4.8	5.7	6.3

West

5.0	6.9	8.4	10.2	12.4	14.4
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Fd. May 1956

I.P. sat Flush  
 9/1/56 →



3.76 1276.46 127.1  
 25 15 8 15 25  
 149+00 5.0 5.0 4.6 4.4 4.2 3.9

1271.9  
 25 15 8 15 25  
 150+00 5.4 5.3 4.9 4.6 4.2 3.9

1271.7  
 25 14 9 12 25  
 151+00 5.0 4.7 5.7 5.3 4.8 5.1 3.9 3.8

1271.2  
 25 18 10 6 10 19 25  
 152+00 6.1 5.5 6.1 5.3 5.6 5.7 4.6 4.7

1270.4  
 25 14 10 4 8 13 18 25  
 163+00 6.4 6.8 7.0 6.0 6.5 7.0 6.5 5.3 5.3

1269.0  
 25 14 8 8 15 25  
 154+00 7.7 8.1 8.2 7.5 8.0 7.7 7.4  
 7.40 1269.06

X 1537 X

X

X

X 154 X

Q180 23 X

Q120 23 18' X

Y 153 Brush X

Q175 23 X

X X 24 X

X X 708 X 21' X 152

X

X

151 X

Q22' X

Q22' 150 X

X Woods +00

18' X

X Brush

149 Y

1271.76

2.70 1271.76 1268.1  
 156+00  $\frac{25}{4.3}$   $\frac{11}{4.7}$   $\frac{6}{4.4}$   $\frac{0}{3.7}$   $\frac{4}{4.0}$   $\frac{10}{4.3}$   $\frac{14}{4.2}$   $\frac{25}{4.1}$

1267.2  
 156+00  $\frac{25}{6.0}$   $\frac{17}{5.7}$   $\frac{8}{5.5}$   $\frac{8}{4.6}$   $\frac{6}{5.0}$   $\frac{10}{5.0}$   $\frac{25}{5.1}$

Clear Channel  
 156+33  $\frac{153}{8.2}$   $\frac{100}{26.7}$   $\frac{50}{5.7}$   $\frac{FL}{4.9}$   $\frac{1266.9}{6.8}$   $\frac{FL}{6.8}$

157+00  $\frac{25}{5.8}$   $\frac{18}{5.5}$   $\frac{9}{5.3}$   $\frac{2}{4.8}$   $\frac{15}{5.1}$   $\frac{25}{5.0}$   $\frac{25}{4.8}$   
 B.M. = 15 1268.39 record  
 3.38 1268.38

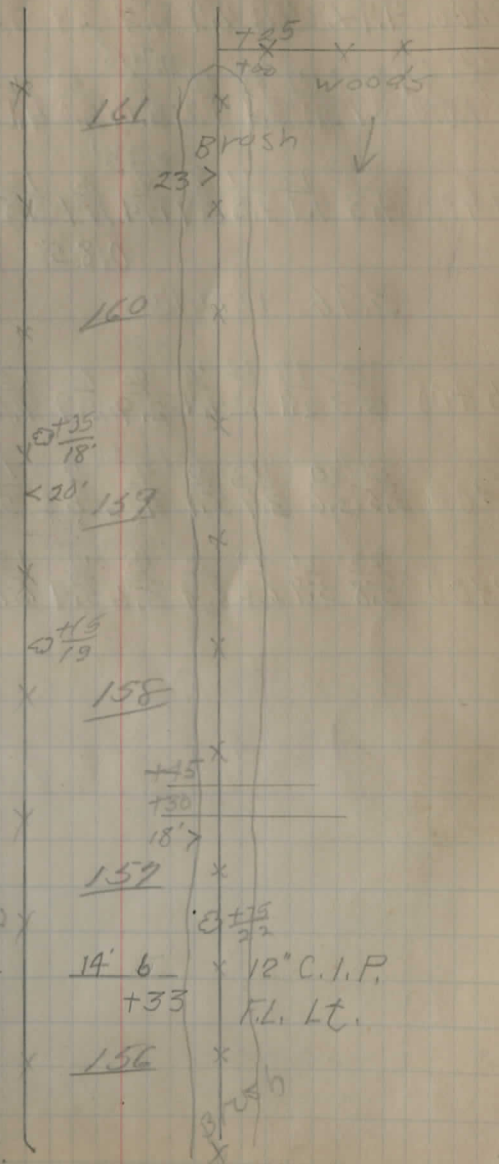
6.14 1274.52

1268.0  
 158+00  $\frac{25}{6.4}$   $\frac{19}{6.4}$   $\frac{13}{6.5}$   $\frac{11}{7.9}$   $\frac{4}{6.5}$   $\frac{4}{6.5}$   $\frac{8}{8.0}$   $\frac{9}{6.6}$   $\frac{13}{7.3}$   $\frac{14}{6.5}$   $\frac{19}{5.3}$   $\frac{25}{5.1}$

1269.2  
 159+00  $\frac{25}{5.8}$   $\frac{19}{5.5}$   $\frac{13}{5.9}$   $\frac{13}{6.7}$   $\frac{5}{5.5}$   $\frac{4}{5.3}$   $\frac{6}{6.6}$   $\frac{8}{5.4}$   $\frac{11}{5.8}$   $\frac{14}{4.9}$   $\frac{25}{4.9}$

1269.9  
 160+00  $\frac{25}{5.5}$   $\frac{19}{5.2}$   $\frac{13}{4.6}$   $\frac{11}{5.0}$   $\frac{5}{4.6}$   $\frac{5}{5.5}$   $\frac{10}{5.2}$   $\frac{17}{5.2}$   $\frac{22}{4.0}$   $\frac{25}{4.0}$

1270.2  
 161+00  $\frac{25}{5.2}$   $\frac{18}{4.8}$   $\frac{13}{4.9}$   $\frac{9}{5.6}$   $\frac{4}{4.3}$   $\frac{5}{4.3}$   $\frac{11}{5.7}$   $\frac{13}{4.9}$   $\frac{18}{4.9}$   $\frac{21}{4.0}$   $\frac{25}{4.0}$



change to 18"  
 could run 12" VSPX  
 clay channel.  
 200'

1274.52

1276.8

162+00  $\frac{25}{4.7} \frac{14}{4.3} \frac{5}{4.3} \frac{2}{4.9} \frac{3}{5.7} \frac{11}{3.7} \frac{14}{5.0} \frac{18}{4.1} \frac{25}{4.0} \frac{25}{3.4}$

1271.5

163+00  $\frac{25}{3.4} \frac{17}{3.1} \frac{9}{3.4} \frac{7}{4.2} \frac{5}{5.0} \frac{11}{3.0} \frac{13}{4.1} \frac{18}{3.2} \frac{25}{3.1} \frac{25}{2.4}$

1273.1

164+00  $\frac{25}{1.3} \frac{18}{1.1} \frac{11}{1.3} \frac{8}{3.9} \frac{2}{1.4} \frac{6}{1.4} \frac{13}{2.5} \frac{14}{1.8} \frac{25}{-0.2}$

0.85 1273.67

3.96 1277.63

1274.7

165+00  $\frac{25}{3.3} \frac{17}{2.9} \frac{16}{3.2} \frac{7}{2.4} \frac{2}{4.4} \frac{6}{2.9} \frac{13}{4.2} \frac{16}{2.8} \frac{20}{2.4} \frac{25}{2.4}$

1273.4

166+00  $\frac{25}{3.5} \frac{0}{3.6} \frac{13}{3.9} \frac{9}{5.1} \frac{2}{4.2} \frac{7}{4.3} \frac{13}{5.6} \frac{15}{4.7} \frac{19}{4.5} \frac{20}{3.1} \frac{25}{2.9}$

1272.0

167+00  $\frac{25}{5.8} \frac{31}{5.9} \frac{14}{6.2} \frac{8}{6.9} \frac{2}{5.6} \frac{7}{5.4} \frac{13}{6.6} \frac{16}{5.6} \frac{21}{5.1} \frac{25}{5.1}$

27

X

X

X

X

X

X

X

X

X

X

X

X

X

X

X

167

165  
22

166

&lt; 20

23 &gt;

+15

+100

+90

+80

165 +10

+50

164

20 &gt;

Brush

X

X

X

150

163

162

12728

168+00  $\frac{25}{8.8}$   $\frac{19}{2.2}$   $\frac{13}{2.6}$   $\frac{8}{1.1}$   $\frac{4}{4.8}$   $\frac{4}{4.8}$   $\frac{11}{9.0}$   $\frac{19-19}{5.6}$   $\frac{25}{5.6}$

12729

168+07  $\frac{15.8}{9.0}$   $\frac{10.8}{8.7}$   $\frac{5.0}{7.7}$   $\frac{5.6}{3.3}$   $\frac{H}{4.2}$   $\frac{E}{4.7}$   $\frac{4}{4.2}$   $\frac{H}{3.5}$   $\frac{F}{7.8}$

1272.6

169+00  $\frac{25}{5.6}$   $\frac{20}{6.1}$   $\frac{19}{5.5}$   $\frac{8}{4.9}$   $\frac{5}{5.7}$   $\frac{6}{5.0}$   $\frac{11}{4.5}$   $\frac{13}{4.7}$   $\frac{17}{5.4}$   $\frac{25}{4.7}$   $\frac{25}{5.1}$   
1.08 1276.55

9.50 1286.05

1274.6

170+00  $\frac{25}{8.3}$   $\frac{15}{8.9}$   $\frac{8}{10.2}$   $\frac{4}{12.2}$   $\frac{4}{11.4}$   $\frac{4}{11.1}$   $\frac{11}{11.5}$   $\frac{16}{12.7}$   $\frac{18}{11.1}$   $\frac{25}{9.5}$

1276.9

171+00  $\frac{25}{5.4}$   $\frac{19}{2.3}$   $\frac{11}{6.1}$   $\frac{5}{9.7}$   $\frac{4}{9.1}$   $\frac{6}{8.3}$   $\frac{11}{9.1}$   $\frac{14}{10.3}$   $\frac{23-25}{6.2}$

1280.6

172+00  $\frac{25}{3.7}$   $\frac{20}{3.7}$   $\frac{10}{4.4}$   $\frac{7}{6.4}$   $\frac{4}{5.4}$   $\frac{6}{5.5}$   $\frac{13}{9.2}$   $\frac{14}{5.1}$   $\frac{25}{3.7}$

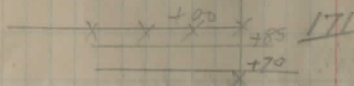
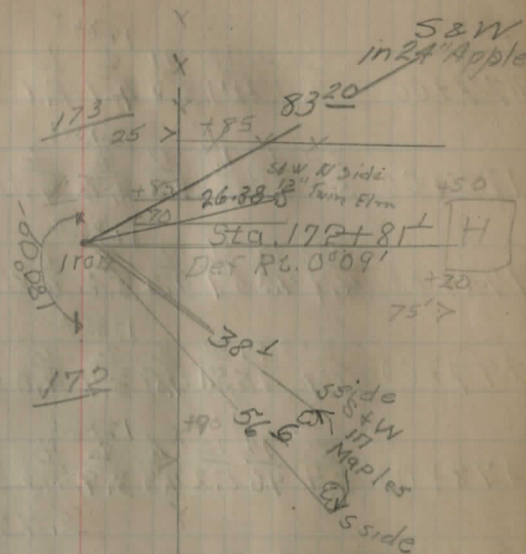
BM 16 2.53 1283.52 1283.52

5.38 1288.90

1283.5

173+00  $\frac{25}{5.5}$   $\frac{14}{5.5}$   $\frac{9}{6.7}$   $\frac{6}{5.8}$   $\frac{4}{5.4}$   $\frac{5}{5.5}$   $\frac{11}{6.5}$   $\frac{14}{5.0}$   $\frac{25}{4.4}$

Fd. May 1956



170  
25

171  
25

172  
25

169

Build new 3x2

Concreted curbing

Height warn

channel

18 15  
77

168

Old Stone Culv.

3x2 Box

FL. LL.

Poor Cond.

1288.90

1284.8  
 25 13 11 4 6 11 14 25  
 194+00 4.9 4.7 5.8 4.1 4.4 5.5 4.2 3.4

1285.3  
 25 13 10 7 8 6 11 13 25  
 175+00 5.1 4.8 5.2 4.3 5.6 4.0 5.0 3.5 2.4

1285.3  
 25 15 11 7 8 6 10 14 25  
 176+00 4.4 4.3 5.1 4.2 3.6 3.8 4.5 2.7 1.8

1285.2  
 25 17 11 8 9 6 11 14 25  
 177+00 5.1 4.8 5.1 4.5 3.7 4.0 4.8 4.3 2.7

1285.4  
 25 14 12 6 8 7 9 11 25  
 178+00 5.4 4.6 5.2 4.3 5.9 4.3 5.2 4.5 2.7

3.95 1284.95

2.67 1287.62

1284.5  
 25 15 13 6 8 5 11 15 25  
 179+00 4.3 4.3 5.1 3.9 3.7 3.7 5.1 3.6 2.8

1283.8  
 25 14 11 6 8 4 10 13 25  
 180+00 4.5 4.6 5.4 4.4 3.8 4.2 5.6 4.5 3.3

29

180

179

178

 $\frac{175}{25}$ 

177

176

 $\frac{170}{20}$ 
 $\frac{170}{20}$ 

174

Brush &amp; small trees

Avoid cutting in front of house!

Hh  
1287.62

1283.2

181+00  $\frac{25}{5.2}$   $\frac{19}{5.3}$   $\frac{11}{5.7}$   $\frac{5}{4.8}$   $\frac{8}{4.4}$   $\frac{4}{4.7}$   $\frac{10}{6.0}$   $\frac{13}{4.7}$   $\frac{25}{4.0}$

1283.1

182+00  $\frac{25}{5.3}$   $\frac{12}{5.3}$   $\frac{9}{6.4}$   $\frac{6}{5.3}$   $\frac{8}{4.5}$   $\frac{6}{4.9}$   $\frac{10}{6.2}$   $\frac{13}{5.4}$   $\frac{25}{4.6}$

1282.3

182+94  $\frac{100}{8.6}$   $\frac{50}{6.8}$   $\frac{FL}{6.6}$   $\frac{2}{5.3}$   $\frac{FL}{6.4}$

1282.4

183+00  $\frac{25}{5.8}$   $\frac{12}{5.4}$   $\frac{11}{6.1}$   $\frac{8}{5.4}$   $\frac{8}{5.2}$   $\frac{4}{5.2}$   $\frac{15}{6.2}$   $\frac{15}{5.4}$   $\frac{25}{5.1}$

1283.8

184+00  $\frac{25}{4.6}$   $\frac{13}{4.3}$   $\frac{11}{5.0}$   $\frac{8}{4.1}$   $\frac{8}{3.8}$   $\frac{1}{4.2}$   $\frac{10}{5.2}$   $\frac{15}{4.0}$   $\frac{15}{4.8}$   $\frac{25}{3.8}$

2.70 1284.92

8.93 1293.85

1284.4

185+00  $\frac{25}{9.4}$   $\frac{13}{9.6}$   $\frac{14}{10.7}$   $\frac{9}{9.8}$   $\frac{8}{9.4}$   $\frac{5}{9.9}$   $\frac{8}{10.8}$   $\frac{14}{9.0}$   $\frac{25}{8.7}$

1286.0

186+00  $\frac{25}{6.9}$   $\frac{16}{8.5}$   $\frac{13}{7.3}$   $\frac{8}{8.1}$   $\frac{8}{9.8}$   $\frac{5}{8.2}$   $\frac{8}{8.1}$   $\frac{14}{7.0}$   $\frac{25}{6.7}$

184

185

184

+75 x x x

26

183

Build new 18"  
VSP Clear Channel  
100 ft

7' 9'

10" Corr. L.P.

+74

F.L. Lt.

182

-100

181 Brush

25

+75

25



1296.76

1297.9

193+22  $\frac{109}{7.3}$   $\frac{50}{6.2}$   $\frac{16}{5.4}$   $\frac{4}{5.9}$   $\frac{FA}{5.1}$

1293.2

194+00  $\frac{25}{4.5}$   $\frac{13}{4.6}$   $\frac{11}{5.2}$   $\frac{8}{4.6}$   $\frac{4}{5.6}$   $\frac{7}{4.3}$   $\frac{11}{5.1}$   $\frac{13}{3.9}$   $\frac{25}{3.6}$

1293.3

195+00  $\frac{25}{4.3}$   $\frac{13}{4.4}$   $\frac{11}{5.2}$   $\frac{8}{4.3}$   $\frac{4}{5.5}$   $\frac{7}{4.0}$   $\frac{11}{4.4}$   $\frac{13}{3.2}$

2.60 1294.16

4.17 1298.33 1293.8

196+00  $\frac{25}{5.8}$   $\frac{13}{5.6}$   $\frac{11}{6.5}$   $\frac{8}{5.5}$   $\frac{4}{4.5}$   $\frac{7}{5.2}$   $\frac{11}{6.1}$   $\frac{13}{4.6}$   $\frac{25}{4.7}$   $\frac{25}{4.1}$

1294.0

197+00  $\frac{25}{5.4}$   $\frac{13}{5.3}$   $\frac{12}{6.3}$   $\frac{8}{5.2}$   $\frac{4}{4.3}$   $\frac{7}{5.2}$   $\frac{11}{6.0}$   $\frac{13}{5.4}$   $\frac{25}{4.6}$   $\frac{25}{3.9}$

1293.5

198+00  $\frac{25}{5.7}$   $\frac{14}{5.7}$   $\frac{12}{6.7}$   $\frac{8}{5.6}$   $\frac{4}{4.8}$   $\frac{7}{5.5}$   $\frac{11}{6.1}$   $\frac{13}{5.2}$   $\frac{25}{4.9}$

1292.3

199+00  $\frac{25}{6.3}$   $\frac{13}{6.4}$   $\frac{6}{7.6}$   $\frac{4}{8.0}$   $\frac{4}{6.0}$   $\frac{7}{6.2}$   $\frac{11}{6.9}$   $\frac{13}{5.4}$   $\frac{25}{4.9}$

1288.8

200+00  $\frac{25}{7.7}$   $\frac{13}{7.5}$   $\frac{6}{8.9}$   $\frac{4}{9.8}$   $\frac{4}{9.3}$   $\frac{7}{9.6}$   $\frac{11}{10.2}$   $\frac{13}{7.9}$   $\frac{25}{7.4}$

BM #18 9.55 1288.74

200

3  $\frac{10}{25}$  199

52 W in  
30 W Maple

Can cut 2' / t

300' B

69.95

198

SEW 5' H

20 W Maple  
5' 4" SE side

SEW 3  
10 W  
Cherry  
S side

27.20

PT STA 197+45.5

Def R F 0° 18'

I.P. Fd. May 1956  
I.P. Sat Flush  
9/8/56

SEW N side  
Tel Pole  
11.2'

52 W in  
8" Ash  
N side

196

195

Said new 12 VSP

194

11' 7'

18" V.S.P.

+22

FL. LT

0.10 1288.84 1285.6  
 201+00  $\frac{25}{2.0} \frac{4}{1.9} \frac{6}{4.4} \frac{4}{3.5} \frac{8}{3.1} \frac{6}{2.7} \frac{11}{3.7} \frac{13}{4.1} \frac{17}{2.7} \frac{25}{1.6}$

1282.5  
 202+00  $\frac{25}{4.6} \frac{11}{4.9} \frac{7}{7.8} \frac{3}{6.7} \frac{3}{6.3} \frac{4}{6.1} \frac{8}{6.8} \frac{12}{7.4} \frac{17}{5.0} \frac{20}{4.3}$

1279.4  
 203+00  $\frac{23}{7.4} \frac{14}{7.5} \frac{8}{10.3} \frac{9}{9.4} \frac{3}{9.2} \frac{9}{9.7} \frac{13}{10.5} \frac{17}{7.6} \frac{23}{7.2}$   
 11.58 1279.26

0.65 1277.71 1276.9  
 204+00  $\frac{25}{0.0} \frac{4}{0.9} \frac{8}{2.6} \frac{5}{1.4} \frac{8}{1.0} \frac{8}{1.3} \frac{12}{2.3} \frac{12}{0.5} \frac{25}{-1.0}$

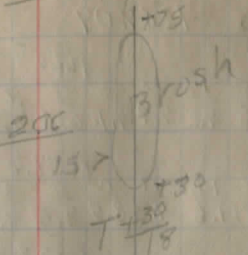
1274.5  
 205+00  $\frac{25}{3.4} \frac{11}{3.3} \frac{8}{4.5} \frac{8}{3.8} \frac{9}{3.4} \frac{9}{3.7} \frac{12}{4.5} \frac{16}{2.4} \frac{25}{2.1}$

1267.7  
 206+00  $\frac{25}{8.0} \frac{19}{7.6} \frac{8}{11.6} \frac{6}{10.9} \frac{8}{10.2} \frac{5}{11.0} \frac{7}{11.5} \frac{10}{9.9} \frac{17}{6.0} \frac{25}{5.4}$   
 11.56 1266.35

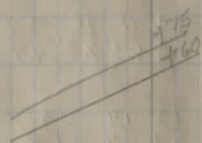
0.60 1266.95 1262.7  
 207+00  $\frac{25}{1.3} \frac{20}{2.4} \frac{12}{4.3} \frac{9}{5.7} \frac{6}{4.8} \frac{9}{4.2} \frac{2}{4.6} \frac{10}{5.1} \frac{14}{4.0} \frac{25}{4.1}$

BM #19 2.55 1264.40 1264.41

202

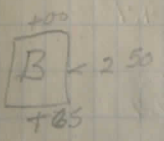


205



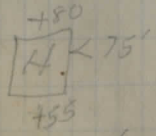
208

T+10/13



203

202



201 T+00/19

① +80/30  
 ② +60/28

2.68 1267.09

1260.5

208+00	23	17	15	5	9	9	15	16	25
	6.6	7.2	7.9	4.1	6.6	7.2	7.9	8.7	9.0

1258.6

208+93	10	30	FL	H	Q	Q	H	FL	
	16.0	14.7	14.6	7.3	8.5	8.5	8.3	7.6	14.9

1258.8

209+00	23	11	5	9	17	23	
	11.3	10.9	8.3	8.5	8.4	10.8	11.1

1259.7

210+00	25	23	13	9	5	10	11	16	25	
	16.2	8.4	7.2	8.0	7.4	6.9	7.2	7.5	7.5	4.9

1264.7

211+00	23	10	4	9	6	13	14	23
	1.0	0.3	3.2	2.4	1.8	2.2	2.7	-1.8

1.02 1266.07

8.90 1274.97 1267.7

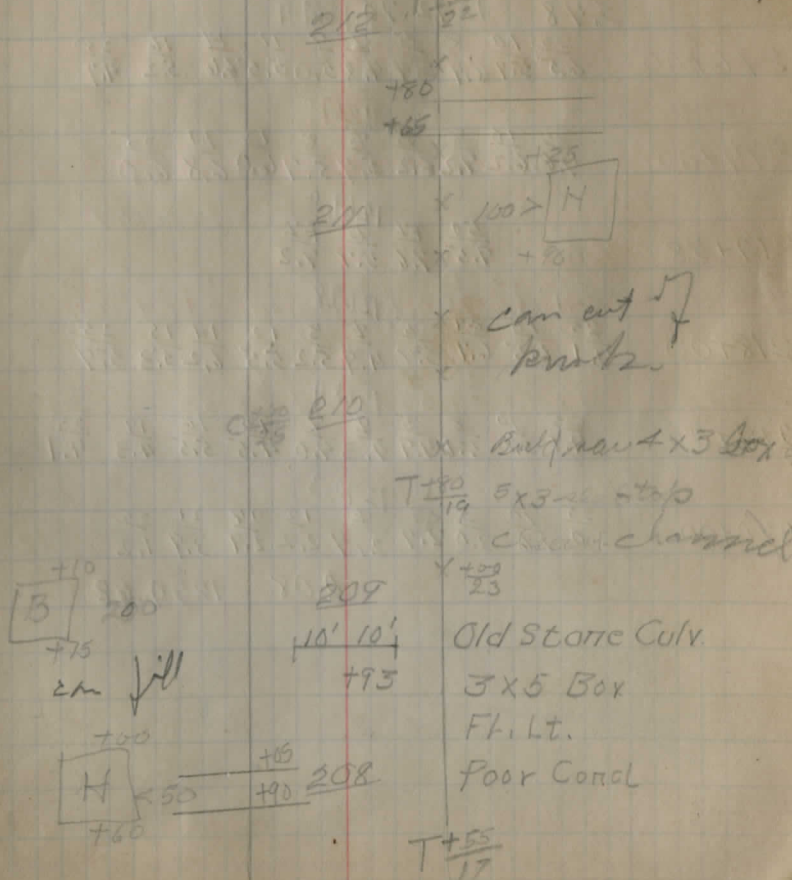
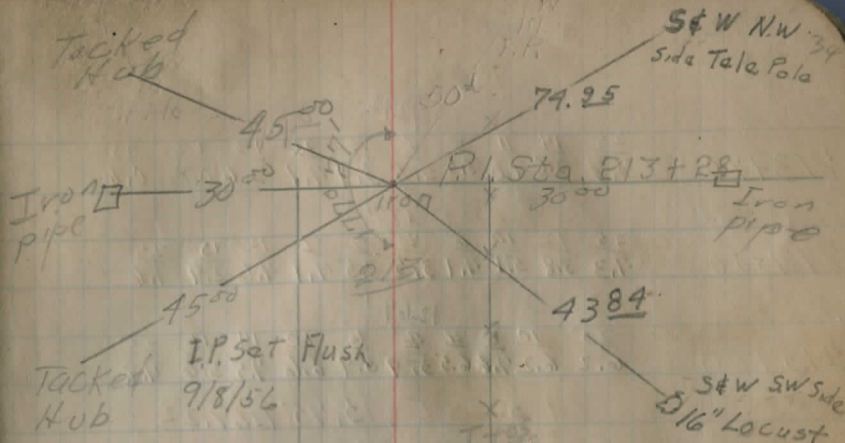
211+50	25	11	9	6	9	13	15	20	25
	7.6	6.8	8.4	8.2	7.3	6.7	7.6	5.6	4.7

1268.9

212+00	25	12	8	6	9	9	13	16	25
	6.7	6.1	7.4	6.8	6.1	7.0	6.8	5.2	4.4

1271.5

213+00	25	14	11	8	6	10	11	14	25	
	3.8	3.0	4.7	4.2	3.5	4.0	4.7	3.5	1.3	0.7



HI  
1274.97  
1272.5

213+00  
 $\begin{array}{r} 25 \\ 3.3 \end{array} \begin{array}{r} 14 \\ 2.8 \end{array} \begin{array}{r} 11 \\ 4.0 \end{array} \begin{array}{r} 8 \\ 3.5 \end{array} \begin{array}{r} 4 \\ 2.5 \end{array} \begin{array}{r} 8 \\ 3.4 \end{array} \begin{array}{r} 11 \\ 4.1 \end{array} \begin{array}{r} 13 \\ 2.6 \end{array} \begin{array}{r} 22 \\ 0.8 \end{array} \begin{array}{r} 23 \\ 0.6 \end{array}$

214+00  
 $\begin{array}{r} 25 \\ 4.3 \end{array} \begin{array}{r} 13 \\ 3.8 \end{array} \begin{array}{r} 10 \\ 3.1 \end{array} \begin{array}{r} 6 \\ 4.1 \end{array} \begin{array}{r} 4 \\ 3.5 \end{array} \begin{array}{r} 5 \\ 3.5 \end{array} \begin{array}{r} 9 \\ 4.1 \end{array} \begin{array}{r} 12 \\ 4.6 \end{array} \begin{array}{r} 13 \\ 2.9 \end{array} \begin{array}{r} 25 \\ 1.6 \end{array}$

215+00  
 $\begin{array}{r} 25 \\ 6.2 \end{array} \begin{array}{r} 10 \\ 6.2 \end{array} \begin{array}{r} 8 \\ 7.6 \end{array} \begin{array}{r} 4 \\ 6.5 \end{array} \begin{array}{r} 4 \\ 5.9 \end{array} \begin{array}{r} 6 \\ 5.9 \end{array} \begin{array}{r} 10 \\ 6.6 \end{array} \begin{array}{r} 14 \\ 7.5 \end{array} \begin{array}{r} 16 \\ 5.6 \end{array} \begin{array}{r} 25 \\ 4.8 \end{array}$

5.75 1269.22

3.48 1272.70 1269.9  
216+00  
 $\begin{array}{r} 25 \\ 6.5 \end{array} \begin{array}{r} 10 \\ 5.9 \end{array} \begin{array}{r} 8 \\ 6.4 \end{array} \begin{array}{r} 5 \\ 5.4 \end{array} \begin{array}{r} 5 \\ 4.5 \end{array} \begin{array}{r} 7 \\ 5.0 \end{array} \begin{array}{r} 11 \\ 5.5 \end{array} \begin{array}{r} 14 \\ 6.6 \end{array} \begin{array}{r} 16 \\ 5.2 \end{array} \begin{array}{r} 25 \\ 4.7 \end{array}$

217+00  
 $\begin{array}{r} 25 \\ 7.6 \end{array} \begin{array}{r} 10 \\ 6.2 \end{array} \begin{array}{r} 8 \\ 7.2 \end{array} \begin{array}{r} 5 \\ 6.2 \end{array} \begin{array}{r} 5 \\ 5.7 \end{array} \begin{array}{r} 8 \\ 5.7 \end{array} \begin{array}{r} 12 \\ 7.6 \end{array} \begin{array}{r} 14 \\ 6.8 \end{array} \begin{array}{r} 25 \\ 6.0 \end{array}$

217+38  
 $\begin{array}{r} 50 \\ 7.5 \end{array} \begin{array}{r} FL \\ 7.6 \end{array} \begin{array}{r} 50 \\ 5.7 \end{array} \begin{array}{r} FL \\ 7.2 \end{array}$

218+00  
 $\begin{array}{r} 25 \\ 7.1 \end{array} \begin{array}{r} 10 \\ 6.5 \end{array} \begin{array}{r} 8 \\ 6.7 \end{array} \begin{array}{r} 5 \\ 5.9 \end{array} \begin{array}{r} 5 \\ 4.9 \end{array} \begin{array}{r} 8 \\ 5.2 \end{array} \begin{array}{r} 12 \\ 5.5 \end{array} \begin{array}{r} 14 \\ 6.2 \end{array} \begin{array}{r} 15 \\ 5.3 \end{array} \begin{array}{r} 25 \\ 5.9 \end{array}$

219+00  
 $\begin{array}{r} 25 \\ 4.9 \end{array} \begin{array}{r} 10 \\ 5.0 \end{array} \begin{array}{r} 8 \\ 5.2 \end{array} \begin{array}{r} 5 \\ 4.9 \end{array} \begin{array}{r} 5 \\ 4.3 \end{array} \begin{array}{r} 9 \\ 4.0 \end{array} \begin{array}{r} 13 \\ 4.5 \end{array} \begin{array}{r} 16 \\ 5.5 \end{array} \begin{array}{r} 19 \\ 4.3 \end{array} \begin{array}{r} 25 \\ 4.1 \end{array}$

220+00  
 $\begin{array}{r} 25 \\ 2.0 \end{array} \begin{array}{r} 10 \\ 1.6 \end{array} \begin{array}{r} 5 \\ 3.0 \end{array} \begin{array}{r} 3 \\ 2.9 \end{array} \begin{array}{r} 5 \\ 2.7 \end{array} \begin{array}{r} 13 \\ 2.7 \end{array} \begin{array}{r} 19 \\ 2.2 \end{array} \begin{array}{r} 21 \\ 3.9 \end{array} \begin{array}{r} 24 \\ 1.2 \end{array}$   
2.08 1290.62

$\begin{array}{r} 120 \\ 5 \\ - 75 \\ + 00 \end{array}$

T  $\frac{40}{27}$

$\begin{array}{r} +90 \\ B \\ - 125 \\ +50 \end{array}$

220

hold near grade.

219

T  $\frac{90}{29}$

Woods

Build new  
15" V. SP Chan.  
channel 50'

6" IR 12" C.I.P.  
+38 FL.Lt.

217-32

T  $\frac{60}{25}$

216

215

T  $\frac{25}{22}$

214  
 $\frac{20}{20}$





1287.77, 1251.9

233+48  $\frac{100}{9.9}$   $\frac{50}{8.6}$   $\frac{FL}{8.3}$   $\frac{E}{5.9}$   $\frac{FL}{8.0}$

234+00  $\frac{23}{6.8}$   $\frac{15}{6.8}$   $\frac{16}{9.3}$   $\frac{13}{6.5}$   $\frac{1281.5}{6.3}$   $\frac{5}{9.6}$   $\frac{6}{6.0}$   $\frac{23}{5.4}$

235+00  $\frac{20}{5.3}$   $\frac{17}{5.4}$   $\frac{12}{6.4}$   $\frac{13}{5.5}$   $\frac{1282.5}{5.3}$   $\frac{6}{6.3}$   $\frac{13}{4.0}$   $\frac{23}{3.5}$

236+00  $\frac{23}{5.4}$   $\frac{E}{5.3}$   $\frac{E}{5.4}$   $\frac{6}{6.3}$   $\frac{8}{5.6}$   $\frac{18}{4.3}$   $\frac{23}{4.2}$

5,05' 1282.92

0.44 1283.16, 1281.8

237+00  $\frac{23}{2.1}$   $\frac{14}{2.5}$   $\frac{13}{3.0}$   $\frac{2}{2.2}$   $\frac{2}{1.4}$   $\frac{9}{2.6}$   $\frac{12}{2.3}$   $\frac{16}{3.9}$   $\frac{23}{0.6}$

238+00  $\frac{23}{3.7}$   $\frac{12}{4.6}$   $\frac{11}{5.5}$   $\frac{E}{4.5}$   $\frac{E}{4.1}$   $\frac{2}{4.6}$   $\frac{9}{5.4}$   $\frac{17}{2.7}$   $\frac{23}{2.3}$

239+00  $\frac{23-15}{6.9}$   $\frac{13}{8.6}$   $\frac{11}{7.9}$   $\frac{6}{8.3}$   $\frac{1275.7}{7.5}$   $\frac{E}{8.3}$   $\frac{5}{9.2}$   $\frac{11}{8.5}$   $\frac{13}{8.2}$   $\frac{17}{6.1}$   $\frac{20-25}{}$

240+00  $\frac{23}{11.0}$   $\frac{15}{11.1}$   $\frac{10}{13.3}$   $\frac{7}{12.3}$   $\frac{1271.6}{11.6}$   $\frac{E}{12.3}$   $\frac{5}{13.2}$   $\frac{11}{12.2}$   $\frac{14}{11.7}$   $\frac{23}{}$

11.37 1271.79

0.12 1271.91 B.M.

BM #22 1.29 1270.62 BM is OK

115 x x x

240

0-18-

6-18-

239

x 20-

238

-25-

spt fd flush 5/66

I.P. sat. Flash

spt fd 3" under

8-25-55

POT Sta 237+00 spike set

Can cut 2' 3/00

237

-25-

42.00

SW Win 24" Maple

SW side

236

+85 +95

+75

+30

520

T 18

235

+95

-25-

234 T 00

16' E' 19

+48 10" V.S.P. FL. LT.



1249.7 1245.5  
 247+00  $\frac{25}{16}$   $\frac{12.15}{8}$   $\frac{4}{8}$   $\frac{5-6}{8}$   $\frac{8}{25}$  ✓  
 4.1 4.2 4.7 3.9 3.8 4.6 4.2 3.3

1244.4  
 248+00  $\frac{25}{15}$   $\frac{13.4}{10}$   $\frac{12}{5}$   $\frac{5}{7}$   $\frac{16-25}{25}$  ✓  
 5.8 5.1 5.9 5.5 4.9 5.9 5.5 5.9

1243.3  
 249+00  $\frac{25}{19}$   $\frac{15-10}{11}$   $\frac{12}{4}$   $\frac{7}{7}$   $\frac{25}{25}$  ✓  
 6.8 6.1 6.9 5.9 6.0 6.8 6.2 6.6

1242.6  
 250+00  $\frac{25}{20}$   $\frac{17-13}{13}$   $\frac{2}{5}$   $\frac{7}{7}$   $\frac{25}{25}$   
 7.0 7.1 8.3 6.9 6.7 8.2 6.9 6.6

1239.7  
 251+00  $\frac{25}{17-15}$   $\frac{14}{2}$   $\frac{5-6}{15}$   $\frac{25}{25}$   
 6.7 10.9 10.0 9.6 9.6 10.1 7.0 6.8

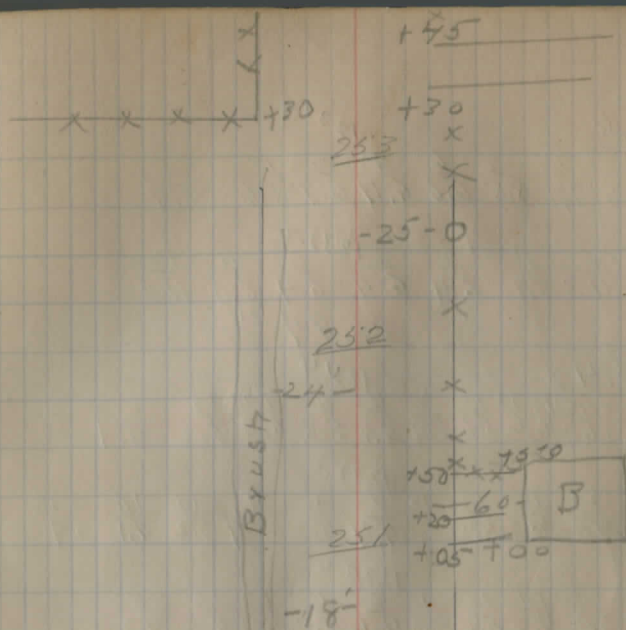
11.37 1237.0

11.68 1239.58 1235.1  
 252+00  $\frac{25}{21}$   $\frac{15}{11}$   $\frac{8}{8}$   $\frac{6}{7}$   $\frac{10}{13}$   $\frac{10}{25}$   
 2.0 2.0 4.3 5.6 4.9 4.5 3.9 4.8 7.9 3.3 0.8 6.4

1233.6  
 253+00  $\frac{25}{13}$   $\frac{10-11}{4}$   $\frac{6}{6}$   $\frac{10}{12}$   $\frac{25}{25}$   
 7.0 6.9 7.4 6.3 6.0 6.4 7.0 6.6 6.8

exists Super P.I curve

6.56	6.36	6.36	6.7	7.1
West	5	10	15	20
				E



250

249

248

247

Row Trees + Brush  
 +50

1955

P.I = 136 + 15.7  
 (242 + 82.7)

D = 15-40

D = 6-00

R = 954.93

PI 136 + 15.70

T 1 31.38

PC 134 + 84.32

L 261.11

P.T 137 + 45.43

E = 9.00

253 389  
 114 11.6 123958 12329

254+100 25 14 5 6 4 2 11 25  
 9.5 9.1 8.8 6.6 6.7 6.9 8.6 9.9

254+9 11.3 5.9 6.4 6.4 6.4 6.4 11.3  
 5.97 1233.2

BM #23 5.97 1233.61 BM150K

3.43 123704 1231.4

253+100 25 15 12 13 10 13 25  
 6.2 6.2 6.6 5.6 5.9 5.6 5.8 6.3 5.2 4.1

1232.6

256+100 25 15 13 13 5 9 11 16 25  
 4.8 5.1 6.0 5.2 4.4 5.2 5.9 5.2 4.1 3.9

1232.4

257+100 25 14 12 9 6 10 12 25  
 5.0 5.2 5.9 5.0 4.6 5.0 5.7 5.2 4.8

1232.8

258+100 25 13 13 11 9 6 9 13 25  
 4.5 4.1 3.7 5.5 4.8 4.2 4.7 5.6 4.2 4.1

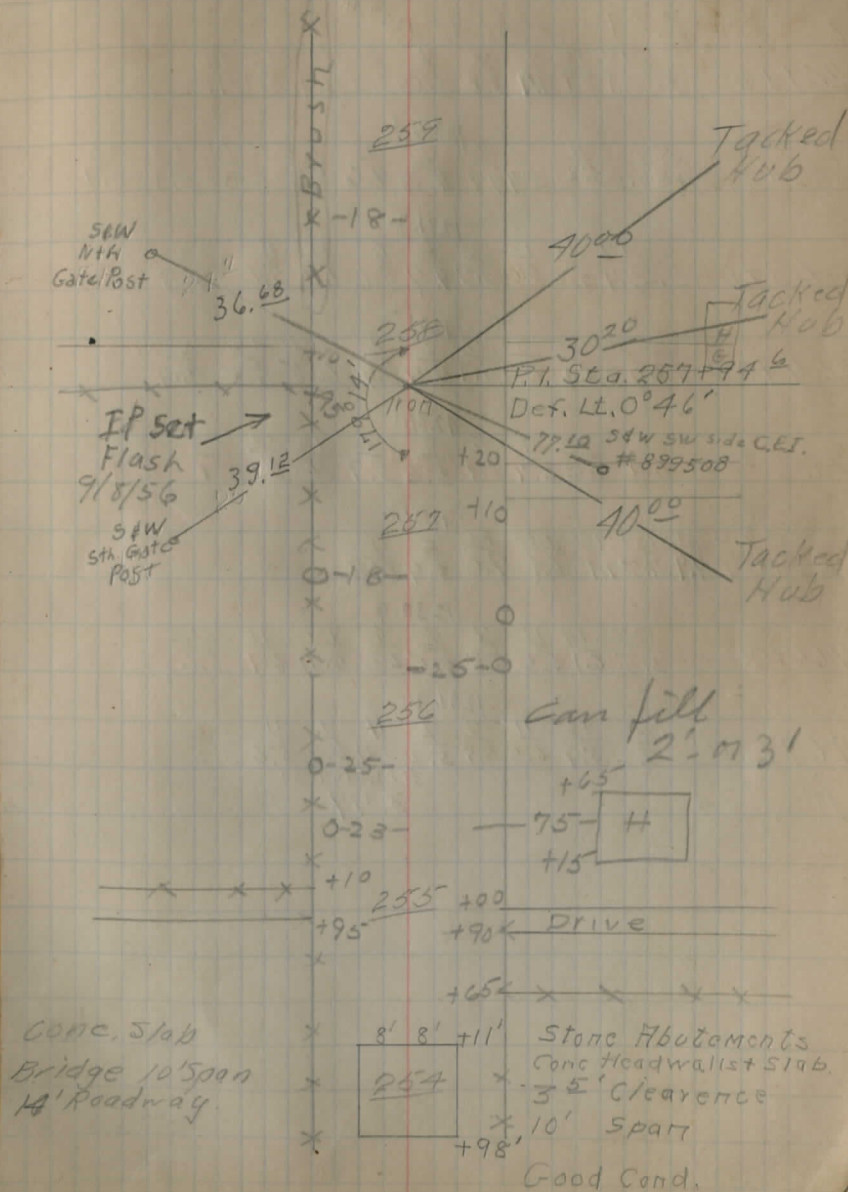
1233.2 OK

259+100 25 13 11 2 9 12 14 25  
 4.2 4.6 5.3 4.7 3.8 4.3 5.6 4.5 4.2

1233.5

260+100 25 13 10 7 9 10 14 25  
 4.1 4.8 5.6 4.7 3.5 4.5 5.5 4.6 4.2

3.67 1233.37



3.01 1236.38 1232.4  
 261+00  $\frac{25}{2.8}$   $\frac{17}{3.1}$   $\frac{11}{3.9}$   $\frac{9}{4.9}$   $\frac{7}{3.8}$   $\frac{8}{5.0}$   $\frac{6}{3.3}$   $\frac{9}{4.4}$   $\frac{13}{5.1}$   $\frac{13}{4.0}$   $\frac{25}{3.8}$

1232.1  
 262+00  $\frac{25}{4.8}$   $\frac{20}{5.5}$   $\frac{11}{5.2}$   $\frac{8}{5.7}$   $\frac{6}{4.9}$   $\frac{8}{4.3}$   $\frac{4}{4.6}$   $\frac{8}{5.3}$   $\frac{11-12}{6.0}$   $\frac{13}{5.1}$   $\frac{25}{5.1}$

1231.7  
 263+00  $\frac{25}{5.2}$   $\frac{17}{5.4}$   $\frac{11}{5.2}$   $\frac{10}{5.8}$   $\frac{8}{5.7}$   $\frac{6}{4.7}$   $\frac{6}{5.6}$   $\frac{9}{6.0}$   $\frac{11}{5.6}$   $\frac{25}{5.9}$

1231.7  
 264+00  $\frac{25}{4.2}$   $\frac{20}{4.3}$   $\frac{13}{6.1}$   $\frac{11}{6.4}$   $\frac{8}{5.7}$   $\frac{6}{4.7}$   $\frac{6}{5.4}$   $\frac{10-11}{6.5}$   $\frac{13}{5.8}$   $\frac{25}{5.4}$

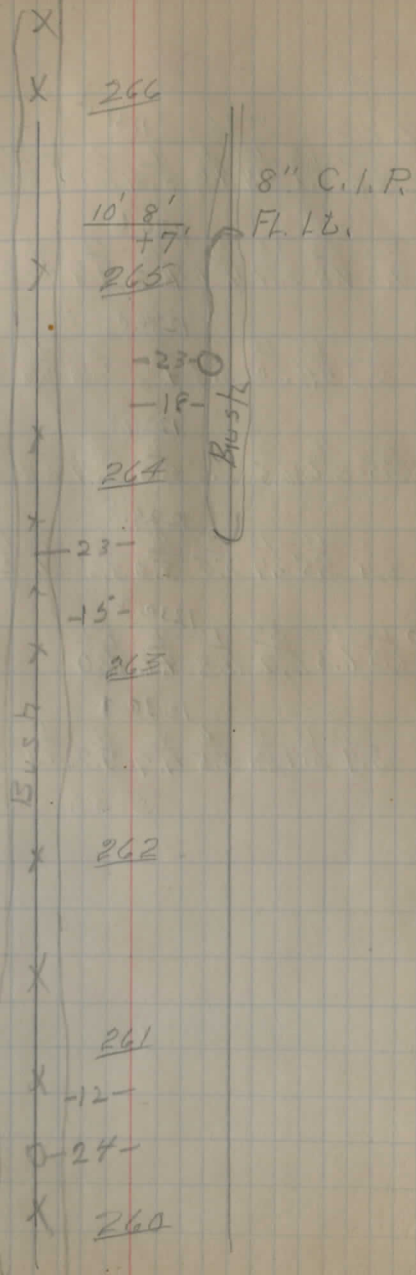
1231.1  
 265+00  $\frac{25}{6.1}$   $\frac{13}{6.3}$   $\frac{9}{6.7}$   $\frac{6}{5.7}$   $\frac{6}{5.3}$   $\frac{6}{5.9}$   $\frac{10-13}{6.5}$   $\frac{13}{6.1}$   $\frac{25}{6.1}$

1231.0  
 265+07  $\frac{25}{8.2}$   $\frac{20}{7.9}$   $\frac{15}{7.5}$   $\frac{10}{7.1}$   $\frac{50}{6.8}$   $\frac{50}{7.0}$   $\frac{FL}{5.4}$   $\frac{FL}{6.6}$

1230.9  
 266+00  $\frac{25}{5.5}$   $\frac{14}{6.1}$   $\frac{11}{6.5}$   $\frac{2}{5.8}$   $\frac{8}{5.5}$   $\frac{6}{6.0}$   $\frac{9-10}{6.7}$   $\frac{11}{6.1}$   $\frac{25}{5.6}$

1231.2  
 267+00  $\frac{25}{5.2}$   $\frac{13}{5.9}$   $\frac{11}{6.5}$   $\frac{2}{5.5}$   $\frac{8}{5.2}$   $\frac{7}{5.7}$   $\frac{9}{6.3}$   $\frac{11}{5.6}$   $\frac{25}{5.2}$

BM #24 3.77 1232.61 BM is OK



Build new 12"  
 VSP lower to flow  
 special ditch

10' 8' + 7'  
 8" C.I.P.  
 FL. L.L.

Bush

Bush

2.22 123483 1231.4  
 268+00  $\frac{25}{3.6}$   $\frac{13}{3.8}$   $\frac{10}{4.9}$   $\frac{10}{4.0}$   $\frac{8}{5.4}$   $\frac{5}{3.8}$   $\frac{2-10}{5.0}$   $\frac{11}{3.8}$   $\frac{25}{6.6}$

1230.6  
 269+00  $\frac{25}{4.3}$   $\frac{13}{4.8}$   $\frac{10}{5.7}$   $\frac{4}{4.7}$   $\frac{8}{4.2}$   $\frac{7}{4.9}$   $\frac{10}{5.5}$   $\frac{12}{4.4}$   $\frac{25}{3.3}$

1230.0  
 270+00  $\frac{25}{5.3}$   $\frac{11}{5.4}$   $\frac{10}{6.0}$   $\frac{2}{5.5}$   $\frac{8}{4.8}$   $\frac{8}{5.3}$   $\frac{10}{5.8}$   $\frac{13}{5.2}$   $\frac{25}{5.0}$

1229.8  
 271+00  $\frac{25}{5.5}$   $\frac{13}{5.6}$   $\frac{7}{6.5}$   $\frac{6}{5.6}$   $\frac{8}{5.0}$   $\frac{7}{5.4}$   $\frac{11}{6.3}$   $\frac{13}{5.4}$   $\frac{25}{5.0}$

1229.8  
 272+00  $\frac{25}{5.4}$   $\frac{11}{5.5}$   $\frac{10}{6.7}$   $\frac{5}{5.5}$   $\frac{8}{5.0}$   $\frac{8}{5.5}$   $\frac{2-10}{6.2}$   $\frac{12}{5.7}$   $\frac{25}{5.5}$

1230.2  
 272+50  $\frac{30}{6.5}$   $\frac{10}{6.3}$   $\frac{10}{6.2}$   $\frac{50}{6.3}$   $\frac{FL}{4.6}$   $\frac{FL}{6.0}$

1230.1  
 273+00  $\frac{25}{5.9}$   $\frac{11}{5.7}$   $\frac{12}{5.7}$   $\frac{6}{5.5}$   $\frac{8}{4.7}$   $\frac{7}{5.2}$   $\frac{13}{6.1}$   $\frac{14}{5.2}$   $\frac{25}{5.5}$   
 5.30 1229.53

Build new 18"  
 VSP down channel  
 500ft

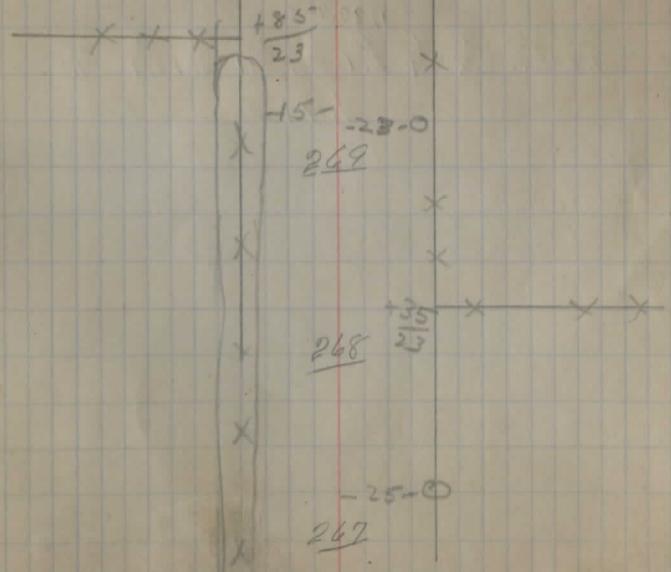
273

7' 9" 10" Carr. in P.  
 +50 Fl. Lt.

272

271

270



775 123728 1230.5  
 274+00  $\frac{25}{24.5}$   $\frac{10}{9.4}$   $\frac{11}{9.3}$   $\frac{10}{8.1}$   $\frac{4}{7.4}$   $\frac{9}{6.8}$   $\frac{11}{7.3}$   $\frac{14}{8.0}$   $\frac{15}{7.2}$   $\frac{18}{7.1}$   $\frac{22}{6.1}$   $\frac{25}{6.0}$

1231.3  
 275+00  $\frac{25}{5.6}$   $\frac{10}{5.7}$   $\frac{13}{6.2}$   $\frac{10}{7.5}$   $\frac{5}{6.6}$   $\frac{9}{6.0}$   $\frac{11}{6.7}$   $\frac{19}{7.8}$   $\frac{23-25}{6.6}$   $\frac{25}{5.1}$

1230.9  
 276+00  $\frac{25}{7.0}$   $\frac{10}{6.7}$   $\frac{5}{9.7}$   $\frac{5}{6.8}$   $\frac{9}{6.4}$   $\frac{8}{6.9}$   $\frac{13}{7.8}$   $\frac{21}{6.7}$   $\frac{25}{6.6}$

1232.4  
 276+00  $\frac{9.0}{2.1}$   $\frac{10.5}{2.7}$   $\frac{10.5}{7.4}$   $\frac{4}{3.5}$   $\frac{6}{4.5}$   $\frac{9}{4.7}$   $\frac{10}{5.0}$   $\frac{11}{3.8}$   $\frac{15}{7.2}$  ← OK OK

1232.2  
 277+00  $\frac{25}{6.3}$   $\frac{9}{5.7}$   $\frac{10}{6.0}$   $\frac{10}{5.6}$   $\frac{10}{5.1}$   $\frac{10}{5.6}$   $\frac{15}{6.4}$   $\frac{21}{6.6}$   $\frac{25}{6.4}$

1233.3  
 278+00  $\frac{25}{3.6}$   $\frac{10}{3.8}$   $\frac{10}{4.7}$   $\frac{10}{4.2}$   $\frac{10}{4.0}$   $\frac{10}{4.4}$   $\frac{11}{4.7}$   $\frac{16}{4.7}$   $\frac{21-25}{4.0}$

1235.2  
 279+00  $\frac{25}{1.2}$   $\frac{10}{2.2}$   $\frac{10}{2.8}$   $\frac{10}{2.4}$   $\frac{10}{2.1}$   $\frac{10}{2.0}$   $\frac{10}{2.7}$   $\frac{14}{2.4}$   $\frac{14}{1.7}$   $\frac{25}{1.5}$   
 1.91 1235.37

Relocated

see pages next after end of this location pg 48

+70 x x x  
 +55 x  
 0  
 0  
 x 20 279  
 0-28-  
 -25-  
 0  
 0  
 278  
 0  
 x  
 x x x +20 -23  
 +10  
 277 x  
 24' WSP  
 culv. in channel 19' 11'  
 +100' LP 300ft x 166  
 296  
 on E side of x 21-  
 with H<sub>2</sub>O in culv.  
 x  
 x  
 x  
 x  
 x  
 274 x

Old Stone Culv.  
 2x2 Box  
 Fl. Lz.  
 Dangerous Corrd.



8/7/28 Richey  
Whiskin  
Spohn

### New Cross Sections

BM #13 1.42 1174.36

1172.94

53+00  $\frac{25}{50} \frac{17}{6.4} \frac{11-12}{87} \frac{10}{7.3} \frac{1167.1}{7.3} \frac{8}{7.2} \frac{11}{6.5} \frac{17}{5.1} \frac{25}{4.1}$  level

52+00  $\frac{25}{76.90} \frac{23}{97} \frac{16}{117} \frac{13}{117} \frac{11}{110} \frac{1163.5}{109} \frac{5}{109} \frac{8}{120} \frac{12}{98} \frac{19}{80} \frac{25}{78}$

13.12 1161.24

2.22 1163.46

51+00  $\frac{25}{1.1} \frac{21}{14} \frac{12}{56} \frac{10}{63} \frac{7}{50} \frac{1159.0}{4.5} \frac{7}{9.7} \frac{9}{5.5} \frac{10}{4.5} \frac{20}{2.0} \frac{25}{1.7}$

50+00  $\frac{20}{6.7} \frac{15}{90} \frac{9}{97} \frac{7.8}{109} \frac{6}{98} \frac{1153.8}{97} \frac{7}{99} \frac{8}{111} \frac{9}{111} \frac{12}{93} \frac{21}{79} \frac{25}{97}$

12.72 1150.74

2.27 1153.81

49+00  $\frac{25}{1.6} \frac{18}{1.3} \frac{6.8}{48} \frac{4}{87} \frac{1149.8}{3.2} \frac{6}{3.6} \frac{7}{4.1} \frac{10}{4.1} \frac{11}{3.6} \frac{15}{2.7} \frac{25}{1.7}$

48+00  $\frac{25}{5.1} \frac{15}{64} \frac{10}{96} \frac{6}{79} \frac{1145.2}{78} \frac{5}{8.2} \frac{9}{20} \frac{14}{6.5} \frac{25}{5.6}$

47+00  $\frac{25}{98} \frac{18}{109} \frac{12}{126} \frac{11}{119} \frac{1141.0}{120} \frac{7}{115} \frac{8}{122} \frac{11}{110} \frac{17}{94} \frac{20}{8.1}$

12.91 1140.10

2.27 1142.37

BM #12 2.83 1139.54 1139.49

2.83 1142.32

### Profile Ohio 168

0+0 1+0 2+0 <sup>3+0</sup> East 4+0 5+0 6+0  
6.0 3.6 1.0 0.1 1.5 2.0 1.8

West  
- 7.1 7.3 7.7 8.4 10.2 12.3

### Typical Sec.

pave 20'  
berm 5'  
ditches 37'

26' tan Lt 40'-45' tan Rt

114232

1136.4

46+00 level  $\frac{21}{25} \frac{20}{6.1} \frac{18}{5.2} \frac{4}{5.9} \frac{5}{5.6} \frac{6}{6.7} \frac{25}{5.6}$  ✓

1134.3

45+00 —  $\frac{25}{8.0} \frac{18}{8.7} \frac{12}{7.7} \frac{4}{8.0} \frac{13}{8.0} \frac{15}{8.7} \frac{17}{8.1} \frac{25}{8.1}$  ✓

1132.7

44+00 —  $\frac{25}{10.0} \frac{21}{10.7} \frac{13}{2.2} \frac{4}{2.6} \frac{10}{2.9} \frac{17}{13.3} \frac{19}{13.3} \frac{20}{11.5} \frac{25}{10.3}$  ✓

10.90 1131.42

251 113393

1130.2 ✓

43+00 —  $\frac{25}{4.5} \frac{16-18}{5.7} \frac{13}{4.3} \frac{4}{3.7} \frac{14}{4.7} \frac{17-19}{6.3} \frac{21}{4.3} \frac{25}{4.1}$  ✓

1128.2 ✓

42+00  $\frac{25}{6.1} \frac{20}{6.1} \frac{16-19}{7.3} \frac{13}{5.7} \frac{4}{5.7} \frac{14}{6.3} \frac{16-19}{7.7} \frac{20}{6.0} \frac{25}{6.0}$

1127.0

41+00 level  $\frac{25}{8.2} \frac{19}{10.5} \frac{16}{10.5} \frac{10}{7.2} \frac{4}{6.9} \frac{18}{8.2} \frac{25}{7.2} - -$

1127.9

40+00  $\frac{25}{10.0} \frac{20}{2.6} \frac{12}{6.4} \frac{4}{6.0} \frac{8}{6.3} \frac{21}{4.8} \frac{25}{1.4}$  level

Relocation Sta 277 to end

✓  
285?

Sta ~~257~~ + 2674 end

$$\begin{array}{r} 285 + 26.74 \\ 106 \quad 67 \\ \hline 178 + 59.74 (1956) \end{array}$$

Sta 282 + 55<sup>25</sup>

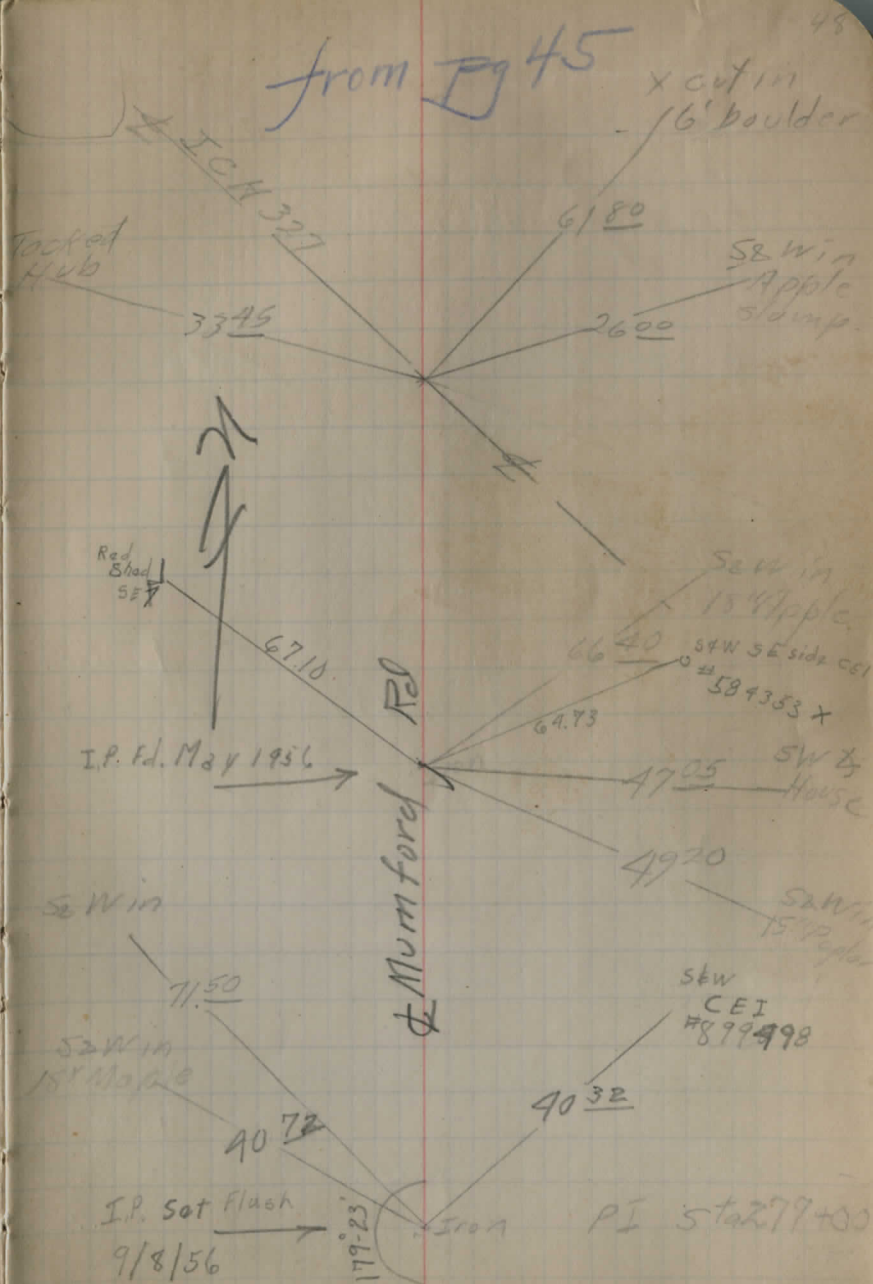
POT

$$\begin{array}{r} 282 + 55.25 \\ 106 \quad 67 \\ \hline 175 + 88.25 (1956) \end{array}$$

Sta 277 + 00

Def. Lt 0°37'

$$\begin{array}{r} 277 + 00 \\ 106 \quad 67 \\ \hline 170 + 33 (1956) \end{array}$$



*[Faint, illegible handwriting on a grid-lined notebook page. The text is mostly obscured by bleed-through from the reverse side.]*



5/15/29  
W. Richey  
P. Richey  
G. Griswold  
P. Ashcraft

Drainage Ditch Location

Sta 12+00

End.

Sta 10+00 4 Left

$549^{\circ}00'W$

Sta 8+00 4 Left

$584^{\circ}50'W$

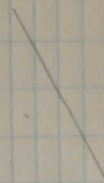
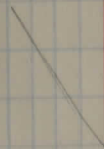
Sta 0+00

$N 80^{\circ} 40' W$

51

Sta 254+00 West

Sidestakes 15' Right or N.



← Munford } { Road Sta 0+00

5-15-27

M. J. ...  
F. ...  
D. ...  
F. ...

## Levels on Drainage Ditch 5+254+00

BM #23	0.96	12340.7		1233.61
Channel E		5.9	1228.2	
" W		5.4	1228.7	
1+00				
2+00				
3+00				
4+00				
5+00				
	2.60	1231.48	5.19	1228.88
6+00				
+90	channel	6.5	1225.0	
7+00				
8+00				
9+00				
10+00			7.9	1223.4
	3.91	1229.68	5.71	1225.97
11+00				

52

$$\frac{40}{4.0} \quad \frac{14}{3.9} \quad \frac{11}{5.1} \quad \frac{8}{5.0} \quad \frac{4}{4.0} \quad \frac{0}{3.7} \quad 1230.4$$

$$\frac{25}{4.6} \quad \frac{0}{4.6} \quad 1229.5$$

$$\frac{30}{5.0} \quad \frac{20}{5.8} \quad \frac{10}{5.7} \quad \frac{0}{5.0} \quad 1229.1$$

$$\frac{30}{5.8} \quad \frac{12}{6.4} \quad \frac{8}{6.9} \quad \frac{6}{6.3} \quad \frac{0}{5.9} \quad 1228.2$$

$$\frac{30}{6.7} \quad \frac{0}{6.4} \quad 1227.7$$

$$\frac{34}{4.9} \quad \frac{26}{6.9} \quad \frac{18}{4.6} \quad \frac{0}{4.3} \quad 1227.2$$

$$\frac{30}{4.6} \quad \frac{0}{4.6} \quad 1226.9$$

$$\frac{30}{5.4} \quad \frac{0}{5.4} \quad 1226.1$$

$$\frac{30}{6.3} \quad \frac{22}{6.7} \quad \frac{17}{7.6} \quad \frac{12}{6.6} \quad \frac{0}{6.4} \quad 1225.1$$

$$\frac{30}{6.4} \quad \frac{20}{6.7} \quad \frac{14}{7.7} \quad \frac{12}{7.5} \quad \frac{0}{6.9} \quad 1224.6$$

$$\frac{30}{5.2} \quad \frac{16}{5.2} \quad \frac{0}{6.1} \quad 1223.6$$

122968

12700		8.0	1221.7
12750		7.7	
13		7.5	
14		8.0	
B.M.		5.11	1224.57
601	1231.78	3.91	1225.77
529	1234.10	2.92	1228.86
B.M. #23		0.51	1233.59

53

$\frac{30}{60}$	$\frac{22}{80}$	$\frac{18}{80}$	$\frac{11}{63}$	$\frac{0}{5.5}$	1224.2
-----------------	-----------------	-----------------	-----------------	-----------------	--------

Top 18" boulder 40' R+L Sta 11750

5/15/29

M Richey  
F Blundy  
G Griswold  
F Ashcraft

Drainage Ditch Location Sta 272+50

Sta 8+00

End.

Sta 7+00

W

Sta 3+00

N 34° 40' W

Sta 0+00

N 76° 40' W

54

Sidestakes 15' Right of N.

↳ Mumford Stone Road

5/19/23

M. J. J. J.  
E. P. J. J.  
G. J. J. J.  
A. J. J. J.

## Levels on Drainage Ditch Sta 272+50.

Temp BM 1.84 1235.34

1233.50

Flow near culvert

7.8 1227.5

1227.5 1227.5 1227.5 1227.5 1227.5 1227.5 1227.5 1227.5 1227.5 1227.5

1 6.8 1228.5

2 7.5 1227.8

3 8.0 1227.3

4 8.8 1226.5

5 9.1 1226.2

6 10.1 1225.2

7 10.9 1224.4

55

E Headwall Culvert Sta 276+66

6/9/29

M. P. P. P.  
+ P. P. P.  
66 Grand  
C. P. P.

BM #7	2.67	1248.68		1246.01
	4.08	1242.56	10.20	1238.48

Flow R			8.44	1234.12	1234.00
Stake R			4.94		C 3.5
Flow L			9.18	1233.38	1233.50
Stake L			5.68		C 3.5

		1242.56		
	0.95	1241.29	2.22	1240.34

Flow R			7.67	1233.62	1233.50
Stake R			5.17		C 2.5
Flow L			8.44	1232.85	1233.00
Stake L			5.94		C 2.5

BM #2	1.72	1111.34		1109.62
-------	------	---------	--	---------

Flow R			12.26	1099.08	1099.2
Stake R			8.26		C 4.0
Flow L			11.62	1099.72	1099.6
Stake L			10.12		C 1.5

No 13

Sta 94+70

Fl. 1233.5				Fl. 1234.20
------------	--	--	--	-------------

C 3.5		18	17	C 3.5
-------	--	----	----	-------

← 19 \* 18 →

No 12

Sta 88+79

Fl. 1233.0				Fl. 1233.5
------------	--	--	--	------------

C 2.5		20	19	C 2.5
-------	--	----	----	-------

← 21 \* 20 →

No 1

Sta 12+60

Fl. 1098.6		23	24	Fl. 1098.2
------------	--	----	----	------------

C 1.5				C 4.0
-------	--	--	--	-------

← 24 \* 25 →

6/25/29

BM #3	4.95	1122.00		1120.05
	0.02	1111.54	10.48	1111.52
	5.81	1108.44	8.81	1102.63
Flow R		11.36	1097.08	1097.2
Stake R		8.86	C.25	
Flow L		10.62	1097.82	1097.7
Stake L		9.12	C.15	

BM #3	1.95	1122.00		1120.05
	0.02	1111.54	10.48	1111.52
Flow R		12.66	1098.88	1099.0
Stake R		10.16	C.2.5	
Flow L		11.92	1099.62	1099.5
Stake L		7.92	C.2.0	

6/29/29

BM #3	1.12	1121.17		1120.05
Flow R		12.49	1108.68	1108.8
Stake R		11.49	C.1.0	
Flow L		11.55	1109.62	1109.5
Stake L		10.05	C.1.5	

57

No 4

Sta 29+3.6

F. 1098.0				F. 1097.5
C. 1.5		22	23	C. 2.5
5'5" offset	←	22	24	4'10" offset

No 5

Sta 26+08

F. 1099.5				F. 1099.0
C. 2.0		21	22	C. 2.5
	←	22	23	→

No 6

Sta 33+39

F. 1109.5				F. 1108.8
C. 1.5		19	20	C. 1.0
	←	20	21	→

6/29/79

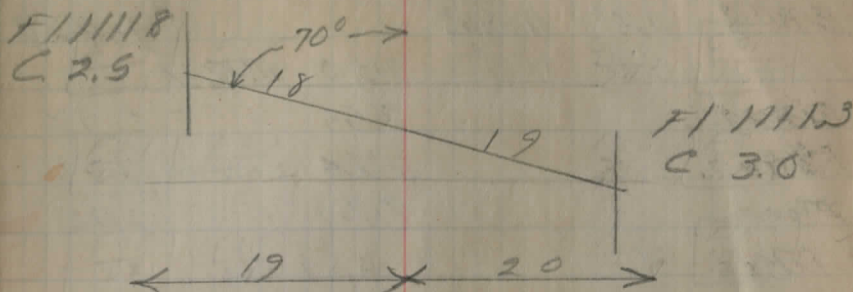
BM #3	1.12	112117		112005
	6.55	111982	790	111327
Flow R			864	1111.18
Stake R			5.64	C30
Flow L			7.90	1111.92
Stake L			5.40	C25

BM #4	0.73	1140.22		113949
	0.56	1132.92	786	1132.3
Flow R			830	1124.62
Stake R	1.35	1113.22	480	C35
Flow L			904	1123.88
Stake L			6.04	C30

BM #5	7.03	1179.97		1172.94
Flow S	1.22	1110.11	5.12	1174.85
Stake S			1.6.25	C3.5
Flow N			2.82	1177.15
Stake N			-0.18	C30

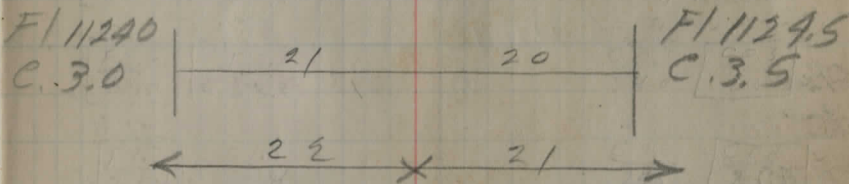
No 7

Sta 36+27



No 8

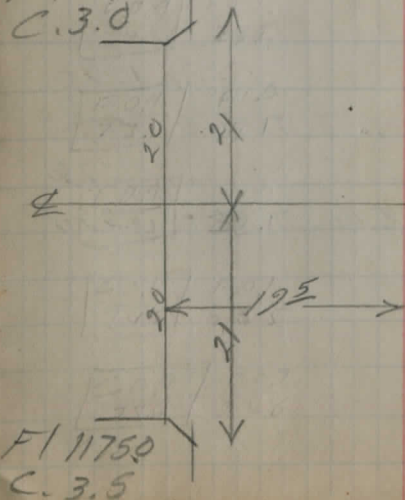
Sta 41+10



F11177.0  
C.3.0

No 10

Sta 57+30



6/29/29

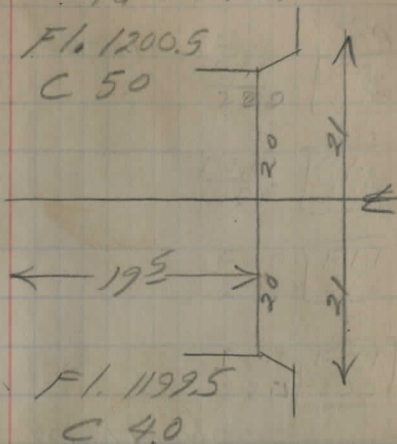
BM#6	2.21	1208.04		12058.3
Flow N		7.40	1200.64	1200.5
Stake N		2.40		C 5.0
Flow S		8.70	1199.34	1199.5
Stakes		4.70		C 4.0

Headwalls only

BM#2	4.65	1114.27	7/2/29	1102.62
Flow N		7.12	1107.15	1107.0
Stake N		2.62		C 4.5
Flow S		8.52	1105.75	1105.9
Stakes		6.02		C 2.5

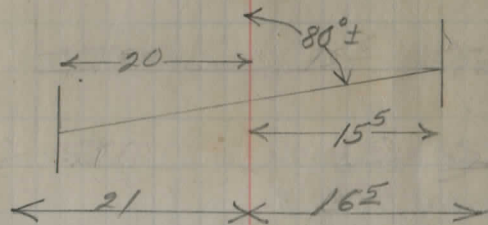
No 11

Sta 66+07

 Fl. 1200.5  
 C 5.0


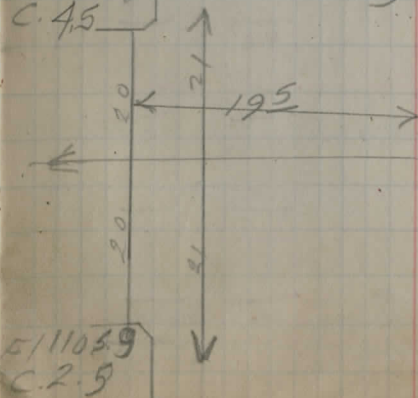
No. 9

Sta 43+45


 Fl. 1107.0  
 C. 4.5

No 3

Sta 16+65



6/28/29

BM#1	177	1120.75		1118.98
0			1.91	1118.84
1			2.96	1117.79
2			4.64	1116.11
3			6.33	1114.42
4	2.06	1116.09	6.72	1114.03
			3.35	1112.74
5			5.04	1111.05

Check Levels to set Bench 7+30

BM#1	0.65	1119.63		1118.98
	0.95	1112.61	7.97	1111.66
New BM 7+30			5.85	1106.76

$\frac{F04}{23.9}$	$\frac{F05}{22.9}$	$\frac{C06}{24.5}$	$\frac{C0.8}{25.5}$
$\frac{F21}{21.1}$	$\frac{F23}{20.2}$	$\frac{F25}{19.9}$	$\frac{F2.3}{20.9}$
$\frac{F09}{23.1}$	$\frac{F10}{22.1}$	$\frac{F05}{22.9}$	$\frac{F0.2}{23.9}$
$\frac{F05}{23.7}$	$\frac{F06}{22.7}$	$\frac{F05}{22.9}$	$\frac{F1.4}{22.9}$
$\frac{F02}{24.2}$	$\frac{F03}{23.2}$	$\frac{C03}{24.0}$	$\frac{C0.3}{25.0}$
$\frac{F13}{22.4}$	$\frac{F15}{21.4}$	$\frac{C06}{24.5}$	$\frac{C0.6}{25.5}$

Spike in Wroot 12' apple 75' L to St 7+30

Robot 6/29/29  
Richey  
Parks  
Cantfield

BM 7150	5.85	1112.61		1106.76
6			3.24	1109.57
7			4.75	1107.86
8			5.89	1106.72
	3.91	1109.74	6.78	1105.83
9			3.81	1105.93
10			4.24	1105.50
11			4.49	1105.25
12			4.61	1105.13
	5.05	1109.38	5.41	1104.33
13			9.10	1105.28
14			3.82	1105.56
15			3.35	1106.03
	8.56	1115.59	2.35	1107.03
16			7.79	1107.80
			5.90	1109.69
				1109.62

$\frac{F1.0}{22.8}$	$\frac{F12}{21.8}$	$\frac{F03}{23.2}$	$\frac{F01}{24.2}$
$\frac{F04}{24.2}$	$\frac{F03}{23.2}$	$\frac{C08}{24.8}$	$\frac{C09}{25.8}$
$\frac{F09}{23.1}$	$\frac{F10}{22.1}$	$\frac{F04}{23.0}$	$\frac{F03}{24.2}$
$\frac{F09}{22.1}$	$\frac{F10}{22.1}$	$\frac{F12}{21.8}$	$\frac{F11}{22.8}$
$\frac{C01}{24.5}$	$\frac{F01}{23.5}$	$\frac{F07}{22.6}$	$\frac{F05}{23.6}$
$\frac{C07}{25.6}$	$\frac{C07}{24.6}$	$\frac{C01}{23.7}$	$\frac{C00}{24.7}$
$\frac{F11}{23.1}$	$\frac{F10}{22.1}$	$\frac{F11}{22.0}$	$\frac{F0.8}{23.0}$
$\frac{F17}{22.1}$	$\frac{F17}{22.1}$	$\frac{F20}{20.6}$	$\frac{F1.8}{21.6}$
$\frac{F1.0}{23.1}$	$\frac{F10}{22.1}$	$\frac{F20}{20.6}$	$\frac{F2.1}{21.6}$
$\frac{C03}{23.0}$	$\frac{C03}{24.0}$	$\frac{F09}{22.3}$	$\frac{F1.0}{23.3}$
$\frac{C02}{24.9}$	$\frac{C02}{23.9}$	$\frac{F06}{22.7}$	$\frac{F0.5}{23.7}$

BM#2 5.90 1115.52 110962

17		4.65	1110.87
18	8.35	1122.33	1.54 1113.98
		8.21	1114.12
19		5.37	1116.96
20		5.47	1116.86
21		8.51	1113.82
22	1.56	1114.08	9.81 1112.52
		3.71	1110.37
23		6.99	1107.09
24		9.10	1104.98
25	5.09	1109.06	10.11 1103.97
		4.82	1104.24
26		4.21	1104.85
27		2.23	1106.82
28	11.81	1120.42	0.45 1108.61
		10.42	1110.00

$\frac{F1.1}{23.1}$   $\frac{F1.0}{22.7}$

$\frac{25}{-}$

$\frac{F4.0}{22.9}$   $\frac{F3.9}{21.9}$

$\frac{C1.6}{26.0}$   $\frac{C2.1}{27.0}$

$\frac{C0.0}{24.3}$   $\frac{F0.2}{23.3}$

$\frac{C1.0}{25.1}$   $\frac{C0.8}{26.1}$

$\frac{C1.0}{25.8}$   $\frac{C0.8}{24.8}$

$\frac{C0.9}{24.9}$   $\frac{C0.9}{25.9}$

$\frac{C2.1}{27.6}$   $\frac{C2.0}{26.6}$

$\frac{C2.4}{27.2}$   $\frac{C2.8}{28.2}$

$\frac{F6.7}{28.0}$   $\frac{F6.3}{27.0}$

$\frac{F2.9}{19.9}$   $\frac{F2.8}{20.9}$

$\frac{F1.9}{21.6}$   $\frac{F2.0}{20.6}$

$\frac{F1.5}{21.4}$   $\frac{F1.3}{22.4}$

$\frac{F1.0}{22.8}$   $\frac{F1.2}{21.8}$

$\frac{F1.7}{21.1}$   $\frac{F1.7}{22.1}$

$\frac{F0.5}{22.6}$   $\frac{F0.7}{22.6}$

$\frac{F0.9}{22.3}$   $\frac{F0.8}{23.2}$

$\frac{F3.5}{22.5}$   $\frac{F2.7}{21.5}$

$\frac{F4.0}{22.7}$   $\frac{F4.5}{23.7}$

$\frac{F2.1}{21.5}$   $\frac{F2.1}{20.5}$

$\frac{F2.8}{19.7}$   $\frac{F2.8}{20.7}$

$\frac{C3.8}{30.0}$   $\frac{C3.6}{29.0}$

$\frac{C0.3}{24.0}$   $\frac{C0.8}{25.0}$

112042

29 7.09 111333

30 3.56 111666

31 2.04 1118.38  
 6.53 112303 3.92 111650

BM#3 2.73 1122.78 2.73 1120.30 1120.05

New BM 1.90 1120.88

32 5.92 1116.86

33 1113.95

34

$\frac{C24}{28.0}$   $\frac{C23}{27.0}$

$\frac{C1.1}{25.2}$   $\frac{C1.4}{26.2}$

$\frac{C0.8}{25.9}$   $\frac{C0.9}{24.9}$

$\frac{F0.5}{22.9}$   $\frac{F0.4}{23.9}$

$\frac{C0.9}{25.8}$   $\frac{C0.8}{24.8}$

$\frac{F1.1}{20.5}$   $\frac{F1.9}{21.5}$

Spike in Eroct 18" Maple 125' 1/4 Sta 31+10

$\frac{C4.0}{29.6}$   $\frac{C3.9}{28.6}$

$\frac{F7.2}{28.5}$   $\frac{F7.9}{29.5}$

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7/5/29

 R. P. Wilson  
 E. Parks  
 C. Confield  
 V. Hoffman

BM #4	10.9	114053		1139.49
42			10.03	1130.50
New BM			4.23	1136.30
43			8.40	1132.13
44			6.77	1133.76
45			5.03	1135.50
46			2.39	1138.14
BM #4	11.09	115058	1.04	1139.49
47			8.79	1141.79
48			4.24	1146.34
	11.85	116229	0.14	1150.44
49			11.29	1151.00
50			6.62	1155.67
51			1.96	1160.33
	11.11	117332	0.08	1162.21
52			8.77	1164.55
53			5.44	1167.88

$\frac{F29}{21.1}$	$\frac{F30}{20.1}$	$\frac{F28}{19.7}$	$\frac{F29}{20.7}$
Spike in Wroot 42' Maple 75 R/d St 44.15			
$\frac{F31}{21.5}$	$\frac{F32}{20.5}$	$\frac{F24}{20.0}$	$\frac{F2.5}{21.0}$
$\frac{F20}{21.6}$	$\frac{F20}{20.6}$	$\frac{F30}{20.1}$	$\frac{F2.6}{21.1}$
$\frac{F16}{22.2}$	$\frac{F16}{21.2}$	$\frac{F15}{21.4}$	$\frac{F1.4}{22.4}$
$\frac{F18}{21.9}$	$\frac{F18}{20.9}$	$\frac{F17}{21.1}$	$\frac{F1.6}{22.1}$
$\frac{C1.8}{27.1}$	$\frac{C1.7}{26.1}$	$\frac{C2.4}{27.2}$	$\frac{C2.5}{28.2}$
$\frac{C1.5}{26.5}$	$\frac{C1.3}{25.5}$	$\frac{C1.1}{25.2}$	$\frac{C1.3}{26.2}$
$\frac{C1.0}{25.9}$	$\frac{C0.9}{24.9}$	$\frac{C0.3}{24.0}$	$\frac{C0.8}{25.0}$
$\frac{C1.3}{26.2}$	$\frac{C1.1}{25.2}$	$\frac{C0.1}{23.7}$	$\frac{C0.2}{24.7}$
$\frac{C2.5}{28.5}$	$\frac{C2.6}{27.5}$	$\frac{C1.3}{25.5}$	$\frac{C1.5}{26.5}$
$\frac{C2.1}{27.4}$	$\frac{C1.9}{26.4}$	$\frac{C1.8}{26.3}$	$\frac{C1.7}{27.3}$
$\frac{C1.4}{26.4}$	$\frac{C1.2}{25.4}$	$\frac{C2.3}{27.0}$	$\frac{C2.4}{28.0}$

		1173.32		
BM#5	0.47	1173.41	0.47	1172.85 1172.74
54			2.65	1170.76
BM#5	7.00	1179.94	0.47	1172.94
55			6.30	1173.64
56			3.42	1176.52
57			0.54	1177.40
T.P. Slope R.			2.16	1177.78
58				1182.28
59				1185.14
60				1188.00
61				1190.50
62				1193.00
63				1195.50
64				1198.00
65				1200.50

$\frac{C0.4}{25.0}$	$\frac{C0.3}{24.0}$	$\frac{C0.1}{23.7}$	$\frac{C0.4}{24.7}$
$\frac{F0.6}{23.7}$	$\frac{F0.6}{22.7}$	$\frac{F0.6}{22.7}$	$\frac{F0.5}{23.7}$
$\frac{F1.6}{21.8}$	$\frac{F1.9}{20.8}$	$\frac{F1.6}{21.2}$	$\frac{F1.4}{22.2}$
$\frac{F1.9}{21.5}$	$\frac{F2.1}{20.5}$	$\frac{F1.9}{20.8}$	$\frac{F1.6}{21.8}$
—	$\frac{21}{}$	$\frac{22}{}$	—
—	$\frac{23}{}$	$\frac{24}{}$	—
—	$\frac{24}{}$	$\frac{24.5}{}$	—
—	$\frac{24}{}$	$\frac{23.5}{}$	—
—	$\frac{25}{}$	$\frac{24.5}{}$	—
—	$\frac{23.5}{}$	$\frac{24}{}$	—
—	$\frac{24.5}{}$	$\frac{24}{}$	—

7-7882-C

7-5587

242182

274

111817

98864

11

111817

# Bench Mark Check Levels

B.M. #2 Grove Corners Sta. 16+80

Elev. 1109.62

6.61 1116.23

0.36 1118.87

4.07 1119.94

12.63 1107.31

1.98 1109.29

3.48 1105.81

12.08 1117.89

0.59 1117.30

3.83 1121.13

1.08 1120.05

B.M. #3

9.30 1111.83

10.24 1122.07

0.99 1121.10

10.84 1131.94

0.23 1131.71

8.17 1139.88

2.15 1137.73

6.53 1144.26

B.M. #4

4.77 1139.49

B.M. #4

0.44 1143.82

66  
Spike in root 30" Maple 60' Lt &

Spike in E. Side 12" Locust 25' Lt & Sta. 32+50

Spike in root of 15" Locust 20' RL & Sta. 46+45

12.59 1156.41  
1.57 1154.84

11.85 1166.69  
0.76 1165.93

9.25 1175.18  
2.24 1172.94

0.44 1174.748  
8.76 1183.50

0.36 1183.14  
12.92 1196.06

2.77 1193.29  
10.02 1203.31

2.10 1201.21  
7.38 1208.59

2.76 1205.83  
3.11 1208.94

0.36 1208.68  
8.11 1216.69

0.55 1216.14

BM #5

BM #6

SPike in root 48" Locust 25' R & 54' S

SPike in root 20" Maple 30' R & +30' N.  
of road leading E. at Sta. 66+35

8.23 1224.37  
BM #7 4.64 1219.73

12.70 1235.36  
1.34 1234.02

8.54 1242.56  
BM #8 5.28 1237.28

7.77 1243.41  
6.92 1235.64

7.89 1244.88  
1.49 1243.39

6.05 1249.44  
BM #9 3.43 1246.01

5.11 1249.03  
8.17 1240.86

4.63 1245.49  
6.45 1239.04

Spike in root 30" Maple 25' RL & Sta. 95+00

Spike in root 30" Maple 50' Lt & Sta 89+00

Spike in root 12" Maple 25' RL & Sta. 98+65

Spike in root 18" Maple 20' Lt & 106+00

5.60 1244.64

BM #11

1.12 1243.52

BM

Spike in root of spreading Elm 35' Lt C  
Sta. 114+00

1.81 1242.83

11.56 1254.39

0.00

8.98 1263.37

0.18 1263.19

Spike in root of 10" Cherry 25' Rt C  
Sta. 125+30

9.17 1272.36

BM #12

4.09 1268.29

4.95 1273.22

2.20 1271.02

4.22 1275.24

0.64 1274.60

5.78 1280.38

BM #13

2.25 1278.13

Spike in root of 10" Cherry 20' Rt C  
Sta. 141+60

0.90 1279.03

BM #14

6.33 1272.00

Spike in root of 15" Maple 20' Lt C  
Sta. 148+10

3.35 1276.05

6.02 1270.03

B.M.	2.00	1272.03	18"	Maple	30'	St.
	5.32	1266.71				
	6.80	1273.51				
B.M.#15	5.12	1268.39				
	3.91	1269.60				
	7.92	1277.52				
	5.35	1272.17				
	6.20	1278.37				
	1.31	1277.06				
	7.91	1284.97				
B.M.#16	1.45	1283.52				
	5.43	1288.95				
	4.54	1284.41				
	5.97	1282.97				
	4.04	1287.01				
	3.25	1283.76				
	10.31	1294.07				
	2.05	1292.02				
	5.93	1299.95				
B.M.#17	3.07	1294.88				
	5.25	1292.70				

106+00

Spike in root of 30" <sup>Elm</sup> ~~Basswood~~ 50 Lt & Sta. 158+30

Spike in root of 20" Maple 40 Rt & Sta. 172+20

Spike in root of 20" Cherry 30 Rt & Sta. 190+18

5.25 1297.95

3.14 1296.48

BM#18

0.58 1289.32

0.46 1277.70

0.37 1267.98

BM#19

6.35 1270.76

3.65 1273.71

7.63 1274.02

BM#20

7.63 1281.14

4.61 1293.34

7.74 1288.74

12.08 1277.24

10.09 1267.61

3.57 1264.41

0.70 1270.06

7.32 1266.39

0.51 1273.51

1.50 1278.64

Spike in root 18" Maple 35' Lt &  
Sta. 200+75

Spike in root 24" Maple 30' Lt &  
Sta. 207+50

Spike in root 10" Maple 25' Lt &  
Sta. 220+90

	9.13	1288.77		2.04	1286.73
	3.13	1289.86		5.76	1284.10
BM#21				7.77	1282.09
	4.03	1286.12		2.94	1283.78
	1.99	1285.17		10.49	1274.68
	2.59	1277.27		6.67	1271.40
BM#22				12.00	1260.17
	0.77	1272.17		11.11	1249.87
	0.81	1260.98		6.60	1244.75
	1.48	1251.35			

1279.64  
 7.63  
 1287.27

72

Spike in root 18" Maple 30' Lt 4  
 Sta. 230+05

← For elevation see second page following.

Spike in root 36" Maple 30' Lt 7  
 Sta. 240+50

BM #23 1.70 1246.45 12.12 1234.33

BM #24

BM #25

Check Level to BM #1

BM #2	1.63	1111.25		1109.62
	3.76	1109.06	5.95	1105.30
	6.72	1111.84	3.94	1105.12
	9.05	1119.36	1.53	1110.31
BM #1		0.40	1118.96	✓ 1118.98

73  
For Elevation see next page  
1246.45  
1.70  
1244.75  
East  
X on bridge S.E. cor Headwall Sta 257+00

Spike in root of 12" Maple 25' Rt E  
Sta 267+30.

Spike in root of 10" Maple E side, State Route  
168 100' N.W. of Sta 285+14

1109.62  
 $\frac{30}{88}$   $\frac{100}{88}$   $\frac{150}{9.3}$   $\frac{200}{100}$  channel Rt Sta 12+60

# BM Check Levels

BM 51230+05 ~~3.48~~ 1287.58 1284.10

6.77 1280.81

6.35 1287.16

7.97 1279.19

1.00 1280.19

10.28 1269.91

3.54 1273.45

BM 24050

2.85 1270.60

11.66 1261.79

1.43 1263.22

12.76 1250.46

0.38 1250.84

7.08 1243.76

2.47 1246.23

BM 254+00

12.69 1233.54

3.11 1236.65

3.65 1233.00

3.80 1236.50

5.92 1230.88

4.48 1235.36

BM 267+30

2.85 1232.51

5.84 1229.52

4.76 1234.28

BM #21

BM #22

BM #23

BM #24

123428

082 123346

736 124082

129 123953

110 124063

BM 285+H

849 123214

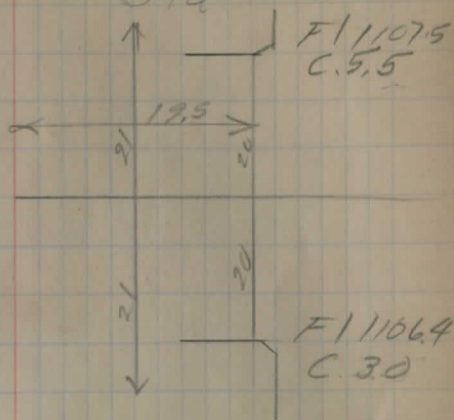
BM #25

7/2/29

BM #2	465	111427	1109.62
Flon N	7.12	110715	1107.0
Stake N	1.62		C 5.5
Flon S	8.52	120575	1205.9
Stake S	5.52		C 30

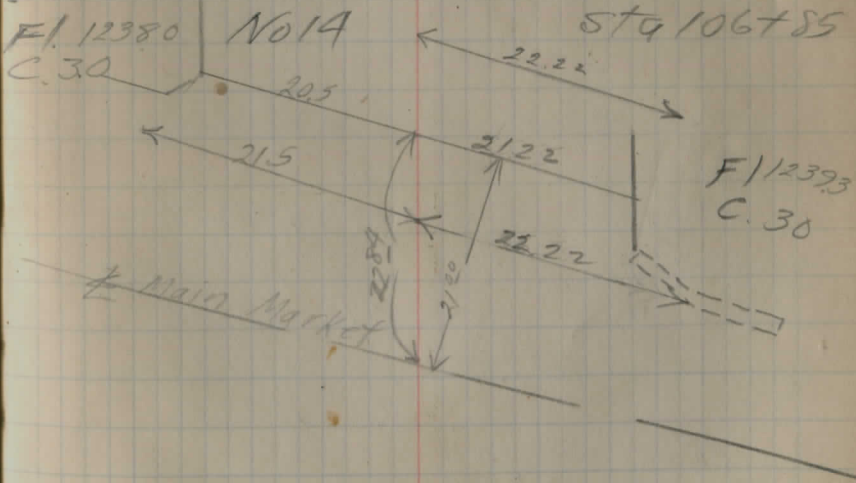
No 2

Sta 16+65



7/14/29

BM #	535	124621	1240.86
Flon E	6.71	123950	1239.30
Stake E	3.71		C 30
Flon W	8.41	123780	1238.00
Stake W	5.41		C 30



7/3/29

Slopes on drainage ditch sta 254+60

Sta	Top	Bottom	Width
0	7.08	1227.00	0.45
1	7.54	1226.54	
2	8.00	1226.08	
3	8.46	1225.62	
4	8.92	1225.16	
5	2.01	1231.48	4.61
			6.78
6	7.24	1224.24	
7	7.70	1223.78	
8	8.16	1223.32	
9	3.51	1229.94	5.05
			7.88
10	7.54	1222.40	
11	7.99	1221.95	
12	8.44	1221.50	
BM 11750	5.41	1224.53	

77

6' Bottom 1/2 to 1 Backslope

C 6.6 Top Wall

$\frac{C40}{9.5}$	$\frac{C3.7}{8.5}$	$\frac{C28}{7.2}$	$\frac{C33}{8.2}$
$\frac{C3.6}{9.1}$	$\frac{C3.4}{8.1}$	$\frac{C31}{7.6}$	$\frac{C3.4}{8.6}$
$\frac{C3.7}{9.2}$	$\frac{C3.5}{8.2}$	$\frac{C3.2}{7.8}$	$\frac{C3.7}{8.8}$
$\frac{C2.7}{7.7}$	$\frac{C2.5}{6.7}$	$\frac{C2.1}{6.1}$	$\frac{2.3}{7.1}$
$\frac{C30}{8.2}$	$\frac{C2.8}{7.2}$	$\frac{C2.7}{7.1}$	$\frac{C3.1}{8.1}$
$\frac{C2.6}{7.6}$	$\frac{C2.4}{6.6}$	$\frac{C30}{7.5}$	$\frac{C3.4}{8.5}$
$\frac{C3.5}{8.5}$	$\frac{C30}{7.5}$	$\frac{C3.2}{7.8}$	$\frac{C3.5}{8.8}$
$\frac{C2.9}{8.1}$	$\frac{C2.7}{7.1}$	$\frac{C2.9}{7.4}$	$\frac{C3.1}{8.4}$
$\frac{C2.6}{6.7}$	$\frac{C2.3}{5.7}$	$\frac{C2.5}{6.6}$	$\frac{C2.6}{7.6}$
$\frac{C2.8}{7.7}$	$\frac{C2.5}{6.7}$	$\frac{C1.6}{5.4}$	$\frac{C2.1}{6.4}$
$\frac{C2.7}{7.6}$	$\frac{C2.4}{6.6}$	$\frac{C2.1}{6.6}$	$\frac{C2.4}{7.6}$
—	$\frac{4.0}{7.0}$	$\frac{C2.5}{6.7}$	$\frac{C2.7}{7.7}$

7/11/29

Staples on Drainage Ditch Sta 277150

BM #24 2.37 12349.0

1232.51

3.53 1232.99 5.44 1229.46

1 6.59 1226.40

2 6.99 1226.00

3 7.39 1225.60

4 7.79 1225.20

5 5.05 1232.14 5.90 1227.09

7.34 1224.80

6 7.74 1224.40

7 8.14 1224.00

2' Bottom 1 1/2 to 1 Backslope

 $\frac{C2.1}{4.0} \frac{C2.0}{4.0}$  $\frac{C2.0}{4.0} \frac{C2.0}{5.0}$  $\frac{C1.7}{4.2} \frac{C1.5}{3.2}$  $\frac{C1.5}{3.2} \frac{C1.6}{4.2}$  $\frac{C1.8}{4.4} \frac{C1.6}{3.4}$  $\frac{C1.6}{3.4} \frac{C1.9}{4.4}$  $\frac{C1.9}{3.2} \frac{C1.5}{3.2}$  $\frac{C1.5}{3.2} \frac{C1.5}{4.2}$  $\frac{C1.4}{4.1} \frac{C1.4}{3.1}$  $\frac{C1.4}{3.1} \frac{C1.5}{4.1}$  $\frac{C0.8}{3.0} \frac{C0.7}{2.0}$  $\frac{C0.7}{2.0} \frac{C0.8}{3.0}$  $\frac{C0.6}{2.8} \frac{C0.5}{1.8}$  $\frac{C0.5}{1.8} \frac{C0.6}{2.8}$

